Photocurrent modelling and experimental confirmation for Meteor Smoke Particle Detectors onboard atmospheric sounding rockets.

Gabriel Giono1,2, Boris Strelnikov1, Heiner Asmus1, Tristan Staszak1, Nickolay Ivchenko2, and Franz-Josef Lübken1

1Leibniz Institute of Atmospheric Physics at the Rostock University (IAP), Kühlungsborn, Germany
2Department of Space and Plasma Physics, School of Electrical Engineering, KTH-Royal Institute of Technology, Stockholm, Sweden.

Correspondence to: G. Giono (ggiono@kth.se)

Abstract. Characterizing the photoelectron current induced by the Sun’s UV radiation is crucial to ensure accurate day-light measurements from particle detectors. This article lays out the methodology used to address this problem in the case of the Meteor Smoke Particle Detectors (MSPDs), developed by the Leibniz Institute of Atmospheric Physics in Kühlungsborn (IAP) and to be flown onboard the PMWE (Polar Meosphere Winter Echoes) sounding rockets in mid-April 2018. The methodology focuses on two complementary aspects: modelling and experimental measurements. A detailed model of the MSPD photocurrent was created based on the expected solar UV flux, the atmospheric UV absorption as a function of height by molecular oxygen and ozone, the photoelectric yield of the material coating the MSPD as a function of wavelength, the index of refraction of these materials as a function of wavelength and the angle of incidence of the illumination onto the MSPD. Due to its complex structure composed of a central electrode shielded by two concentric grids, extensive ray tracing calculations were conducted to obtain the incidence angles of the illumination on the central electrode, and this for various orientations of the MSPD with respect to the Sun. Results of the modelled photocurrent at different heights and for different materials, as well as for different orientation of the detector, are presented. As a pre-flight confirmation, the model was used to reproduce the experimental measurements conducted by Robertson et al. (2014) and agrees within an order of magnitude. An experimental setup for the calibration of the MSPD photocurrent is also presented. The photocurrent induced by the Lyman-alpha line from a deuterium lamp was recorded inside a vacuum chamber using a narrow-band filter, while an UV-sensitive photodiode was used to monitor the UV flux. These measurements were compared with the model prediction, and also matched within an order of magnitude. Although precisely modelling the photocurrent is a challenging task, this article quantitatively improved the understanding of the photocurrent on the MSPD and discusses possible strategies to untangle the MSP current from the photocurrent recorded in-flight.

Copyright statement.
1 Introduction

Meteoric smoke particles (MSP, sometimes also referred as meteor smoke particles) play an important role in the mesosphere/lower thermosphere (MLT) region. They interact with the D- and E-region ionosphere forming the dusty plasma which properties are currently subject of active research. MSPs originate from incoming meteor influx and the estimates of their input to the Earth’s atmosphere ranges from several to hundreds of tons per day (Hughes, 1978; Love and Brownlee, 1993; Ceplecha et al., 1998; Cziczo et al., 2001; Wasson and Kyte, 1987; Mathews et al., 2001; Plane, 2004; Gabrielli et al., 2004; Plane, 2012). Since work of Rosinski and Snow (1961) the term MSP refers to solid state particles which are recondensed from evaporated meteoric material (see e.g., Hunten et al., 1980, for more details). Both these processes (evaporation and recondensation) take place in the height range 70 to 120 km (e.g., Hunten et al., 1980; Love and Brownlee, 1991; McNeil et al., 1998; Kalashnikova et al., 2000; Vondrak et al., 2008; Plane, 2004). The solid particles can further sediment and are even found in the Arctic ice (Gabrielli et al., 2004). The MSPs are also a subject to atmospheric advection and, therefore are influenced by neutral dynamics of the MLT region (see e.g., Megner et al., 2006). It is commonly believed that MSPs could serve as nuclei for heterogeneous nucleation of mesospheric ice particles which cause the strong radar returns known as Polar Mesospheric Summer Echoes (PMSE) (see e.g., review by Rapp and Thomas, 2006). There are a number of works suggesting that MSPs play a key role in formation of the Polar Mesospheric Winter Echoes (PMWE) similar to the mechanism including ice particles in summer for PMSE-formation (e.g., Chen and Scales, 2005; Kavanagh et al., 2006; Belova et al., 2008; Kero et al., 2008; La Hoz and Havnes, 2008; Havnes and Kassa, 2009; Havnes et al., 2011; Mahmoudian et al., 2017). This hypothesis is supported by indirect measurements (e.g., Belova et al., 2008; Kero et al., 2008; La Hoz and Havnes, 2008; Havnes and Kassa, 2009; Havnes et al., 2011), however a verification by direct in-situ measurements is still needed.

Considerable effort was put in the last decades to study the MSP properties (see e.g., reviews by Baumann et al., 2013; Plane et al., 2014). First detected by ion mass spectrometer on board sounding rockets (Arnold and Viggiano, 1982; Arnold et al., 1982; Schulte and Arnold, 1992), their existence was later confirmed by other measurement techniques (Strelnikova et al., 2007; Fentzke et al., 2009; Rapp et al., 2010, 2012; Robertson et al., 2014). Remote sensing techniques as well as modelling rely on some assumptions on MSP’s properties, which are poorly known. Thus, there are many open questions regarding the MSPs, like their size distribution, composition, shape, charge state, work function, photoelectric yield, etc. Microphysical properties of MSPs are difficult to measure because their size varies from tens of nanometers to less than a nanometer. It is known that physical properties of such tiny particles can significantly differ from those, of say µm-size (e.g., Duft et al., 2015).

The most direct measurement technique to study MSPs are the so-called Faraday cup detectors carried by sounding rockets (e.g., Havnes et al., 1996; Rapp and Strelnikova, 2009). These instruments, however are drastically affected by aerodynamics of the rocket flight, prohibiting detection of the smallest particles, normally below 1 nm-size (see e.g., Horányi et al., 1999; Hedin et al., 2005, 2007; Strelnikova et al., 2009; Asmus et al., 2017). To circumvent this limitation, a new rocket-borne MSP-detector (MSPD) was developed at the Leibniz Institute of Atmospheric Physics (IAP) in Kühlungsborn, Germany (Staszak et al., 2017). Its design was inspired by the successful results obtained with the CONE instrument, which was designed as an aerodynamically improved TOTAL instrument (Giebeler et al., 1993; Strelnikov et al., 2013). The MSPD, shown in Figure 1,
consists of a central spherical electrode collecting current from the electrically charged MSPs, shielded by two electrically biased concentric grids (e.g. +6 V and −6 V) repelling the ambient ions and electrons. The geometry was optimized to reduce aerodynamic and bow-shock effects, as these effects directly determine the minimum mass required for the MSPs to reach the central electrode, therefore affecting the estimation of the MSP density. These MSP detectors will be part of a sounding rocket campaign aiming at investigating PMWE, with the first launch schedule in mid-April 2018 from Andøya, Norway.

The photocurrent is another possible limitation of the detector: PMWE are predominantly observed during day-time, so that the measurements need to be conducted under direct sunlight. The photocurrent induced by solar UV radiation on vehicles in the Near-Earth environment is of the order of few nA/cm² (Feuerbacher and Fitton, 1972), which can be few orders of magnitude larger than the current collected from MSPs. The characterization of the expected MSPD photocurrent prior to flight is therefore a crucial aspect of the instrument development, and is presented in detail in this article. The final goal is to provide strategies for interpreting the expected flight measurements, as the recorded current will be the sum of both the MSPs current of interest and the unwanted photocurrent. This endeavour was conducted by means of two distinct, yet complementary, ways: modelling and experimental measurements. An overview of a photocurrent model is presented in Section 2, which includes an atmospheric absorption model for estimating the UV light intensity at various heights, the material properties for various possible surface coating of the detector, and a detailed ray-tracing simulation to quantify the complex illumination on the central electrode depending on the MSPD orientation. The experimental aspect is described in Section 3, where the experimental setup for measuring the MSPD photocurrent is presented. The setup includes a vacuum chamber, a deuterium UV light-source with calibrated spectrum from 115 to 170 nm, a narrow-band filter to select the UV range around Lyman-alpha (121.56 nm) and a UV-sensitive photodiode for monitoring the UV flux. Finally, Section 4 gives a summary of both aspects and discusses ways to utilise them in the prospect of untangling the MSP current from the photocurrent recorded during the flight.
2 Modeling the photocurrent

The photocurrent is the result of the photoelectric effect (Einstein, 1905): high-energy photons at wavelengths from the ultraviolet and below are able to eject electrons from a material when absorbed, as the energy transferred from the photon to the electron is larger than the material work function, giving the excess as kinetic energy to the ejected electron. The photocurrent, i.e. the number of photoelectrons ejected per second, depends on the spectral flux of photon illuminating the material, as well as on the material properties which determine its interaction with the photons.

2.1 Ultraviolet spectral flux as a function of altitude

The first step for estimating the MSPD photocurrent during flight is to determine the spectral flux illuminating the detector as a function of altitude. All photons considered are originating from the Sun, and its UV spectrum is well characterized by spaceborne instruments. The major feature of the solar UV spectrum is the Lyman-alpha line at 121.56 nm, with its spectral intensity being more than two orders of magnitude larger than the UV continuum. The continuum decreases drastically for wavelengths below Lyman-alpha, and as the photocurrent induced by near-UV photons is negligible for most materials, only the spectral region from 115 to 300 nm is considered to be relevant for modelling the MSPD photocurrent. The reference solar UV flux considered for the modelling was taken from the SOLSTICE instrument onboard the SOlar Radiation and Climate Experiment (SORCE) spacecraft (Rottman et al., 2005). This measurement was taken on July 30th, 2006, approximatively one solar cycle ago to roughly represent a similar solar activity as expected during the forthcoming launch. For each height, the number of each spectral photons is reduced by atmospheric absorption depending on the atmospheric column along the photon trajectory.
Atmospheric absorption in the UV is mainly the result of molecular oxygen $O_2$ at heights below 150 km and for wavelength below 200 nm, and of ozone $O_3$ in the whole UV range becoming significant at heights below 70 km. The spectral absorption as a function of height can be estimated knowing the density (as a function of the height) and the absorption cross-section (as a function of the wavelength) for each of these two molecules.

The NRLMSISE-00 atmospheric model (Picone et al., 2002) was used to obtain the atmospheric density of molecular oxygen, following the parameters suggested by the COSPAR international reference atmosphere (CIRA-2012). A low solar and geomagnetic activities scenario was considered as a baseline for the model. Although the atmospheric density of molecular oxygen can vary by up to a factor of two depending on the solar and geomagnetic activities, calculations for both low and high activity scenarios did not show a significant difference in term of the resulting photocurrent. This indicated that the variation of $O_2$ density due to solar and geomagnetic activities does not play a major role in estimating the photocurrent. The atmospheric density of $O_3$ was taken from Bodeker and Hassler (2012), at the latitude of the Andøya rocket launch site in Norway (69.1144°N). Note that the variation of the ozone concentration due to the solar activity was not considered in Bodeker and Hassler (2012) but is not expected to impact significantly the photocurrent estimation since ozone absorption mainly occurs below the altitude of interest for MSP measurements. The absorption cross section for $O_2$ was taken from Blake et al. (1966); Huffman (1985) and from Molina and Molina (1986); Huffman (1985) for $O_3$. It is important to notice that a proper treatment of the Lyman-alpha absorption is crucial for the modelling. For this reason, the precise absorption cross section of $O_2$ at the Lyman-alpha wavelength was taken from Ogawa (1968) and used to the two spectral bins (121 and 122 nm) in which all photons were considered to be from the Lyman-alpha line. This last point is a reasonable assumption, as the UV continuum in this wavelength range is orders of magnitude lower than the Lyman-alpha emission.

Using the atmospheric density $\rho(h)$ and absorption cross-section $\sigma(\lambda)$ of a given species, one can derive the amount of absorption at a given height by first calculating the absorption coefficient $\beta$ at each height

$$\beta(h, \lambda) = \rho(h) \times \sigma(\lambda)$$

The total absorption coefficient $\beta$ is obtained as the sum of all species considered, in the presented case $\beta_{O_2}$ and $\beta_{O_3}$.

The solar zenith angle $\theta_z$ is also an important parameter, as it determines the atmospheric column above a given height. The Earth’s curvature was considered when calculating the atmospheric column, which mostly affects high solar zenith angle condition by reducing the height of the corresponding atmospheric column compared to a classical plan-parallel calculation of the atmosphere. To simulate a realistic atmosphere, the $\beta$ coefficient representing the absorption is derived considering the atmospheric column along the line of sight, which depends on the solar zenith angle $\theta_z$ and the curvature of the Earth. The full geometry of the realistic atmosphere considered is shown in Appendix A.

The absorption optical depth $\tau$ is calculated by integrating the absorption coefficient $\beta$ along the line-of-sight from each given height to the top of the atmosphere $h_{\text{top}}$ (here considered to be 240 km) as shown in Equation (2).

$$\tau(h, \lambda) = \int_{h}^{h_{\text{top}}} \beta(h, \lambda) \, dh$$

(2)
Finally, the number of photons at a given height is derived using the absorption equation

\[ F(h, \lambda) = F(h_{\text{top}}, \lambda) \times e^{-\tau(h, \lambda)} \]  

(3)

where \( F(h_{\text{top}}, \lambda) \) is the solar UV flux at the top of the atmosphere.

Figure 2 shows the computed solar UV flux for various heights and for a solar zenith angle \( \theta_z \) of 75° (around the expected solar zenith angle around mid-day and during spring at the launch site of Andøya). The resulting spectral distributions of photons at various heights are comparable with the ones presented by Huffman (1985).

Note that the contribution from scattered photons was not considered in the calculation. In this part of the atmosphere, the main scattering mechanism is Rayleigh scattering by air molecules (\( N_2 \) and \( O_2 \)) which approximatively scales as \( \lambda^{-4} \). Although one might expect it to be significant for VUV wavelengths, a comparison between the absorption and scattering cross-sections (Bucholtz, 1995) of the major contributors to both effects shows the opposite. Figure 3 shows that the Rayleigh scattering cross-section of air molecules is several orders of magnitude smaller than the absorption cross-section of both \( O_2 \) and \( O_3 \). Hence, absorption by \( O_2 \) should dominate below 120 km, making the scattering from below this height negligible. Scattering from above this height can also be neglected due to the low density of molecules.

2.2 Material properties

The properties of the material are the second important aspect to be considered when estimating the photocurrent, as each material interacts differently with the incoming energetic photons. For any material, knowledge of two properties are required: their photoelectric yield and their reflectance. The photoelectric yield is the probability for a photon with a given energy to eject an electron from the material. Indeed, although all absorbed photons transfer their energy to the electrons inside the material, most of the electrons are only excited inside the material and therefore do not contribute to the photocurrent. The reflectance
Figure 3. Comparison between the absorption cross-section of $O_2$ and $O_3$ with the scattering cross-section of air. Dash lines show the interpolated data.

Figure 4. Photoelectric yield as a function of wavelength for the five different materials: gold, aluminium, stainless steel, graphite and nickel. Dash part of the nickel curve shows the interpolated data.

gives the probability for a photon to be reflected from the material, depending on its angle of incidence $\theta_i$. Reflected photons do not contribute to the photocurrent: only transmitted (i.e. absorbed) photons can transfer their energy to the material electrons.

Photoelectric yields for gold, aluminium, stainless steel and graphite are taken from Feuerbacher and Fitton (1972), and values for nickel up to 180 nm were obtained from Hinteregger and Watanabe (1952). The values used for these five materials are shown in Figure 4. It is important to notice that the photoelectric yield drops by almost two orders of magnitude from 121.5 nm to 250 nm. Hence, even if the solar spectral flux is higher in the near-UV compared to the Lyman-alpha line (see Figure 2), the contribution to the photocurrent from these near-UV photons is expected to be much lower than the contribution from the more energetic Lyman-alpha photons.
The total reflectance $R(\lambda, \theta_i)$ for these materials is the average of the two $R_s(\lambda, \theta_i)$ and $R_p(\lambda, \theta_i)$ reflectances for s and p polarization, respectively, which can be obtained from the Fresnel equations

$$R_s(\lambda, \theta_i) = \frac{\cos \theta_i - n(\lambda) \sqrt{1 - n(\lambda)^{-2} \sin^2 \theta_i}}{\cos \theta_i + n(\lambda) \sqrt{1 - n(\lambda)^{-2} \sin^2 \theta_i}}^2$$

$$R_p(\lambda, \theta_i) = \frac{\sqrt{1 - n(\lambda)^{-2} \sin^2 \theta_i} - n(\lambda) \cos \theta_i}{\sqrt{1 - n(\lambda)^{-2} \sin^2 \theta_i} + n(\lambda) \cos \theta_i}^2$$

where $n(\lambda)$ is the refractive index of each material as a function of wavelengths. Measurements of $n(\lambda)$ for gold, aluminium, graphite and nickel were taken from Hagemann et al. (1975), McPeak et al. (2015), Djurisic and Li. (1999) and Werner et al. (2009), respectively. Proper measurements of the index of refraction for stainless steel in the UV were not found in the literature, and values for iron measured by Werner et al. (2009) were used instead.

The transmittance is obtained as $T(\lambda, \theta_i) = 1 - R(\lambda, \theta_i)$. Figure 5 shows a comparison of the reflectance at Lyman-alpha for the five difference materials.

2.3 Illumination on the detector

A proper knowledge of the illumination’s angle of incidence $\theta_i$ onto the MSPD is required for estimating the photocurrent. Ray-tracing simulations can provide a quantitative estimation of illumination across the detector surface given that a high enough spatial resolution for the grid is used. However, due to its complex geometry, modelling the instrument in a standard ray-tracing software was not possible and a custom routine was created instead. The central electrode was modelled as a sphere, and each wire composing the two concentric grids (hereafter referred as grid-wire) was modelled as a torus (98 in total). The ray-tracing calculations aimed at finding the intersection between a given ray (i.e. a vector) and each of the instrument surfaces.
by solving a quartic equation for each torus, and one quadratic equation for the central sphere. The resolution of the simulated grid of rays was 0.1 mm, which is small enough compared to the radius of the grid-wire radius (0.5 mm). In addition, only half of the MSPD was simulated thanks to symmetry, \textit{i.e.} X-axis from 0 to +45 mm, and Z-axis from –45 to +45 mm. Although the MSPD is symmetric along two of its axes, a change in inclination (\textit{i.e.} rotation of the detector around one of the two axes of symmetry) can result in a different illumination of the central electrode. This was investigated by performing calculation for seven different inclinations, from 0° to 90°. Such simulations are quite computationally-intensive: each run at a given inclination was composed of approximately 320,000 rays and required about a week of computation on a 24-CPU node from the KTH PDC post-processing server. Figure 6 shows the resulting illumination for three different inclinations: 0°, 45° and 90°. Rays interacting with the central electrode are shown in red in Figure 6, and their angle of incidence with respect to the sphere can easily be obtained using the output from the ray-tracing simulation.

### 2.4 Resulting photocurrent

The MSPD photocurrent can be obtained by combining how the UV photons at each height (Section 2.1) fall on the detector (Section 2.3) and interacts with its material (Section 2.2). The resulting photocurrent as a function of height is shown in Figure 7 for the five different materials at a 0° inclination. As expected from its photoelectric yield, a carbon coating produces the lowest photocurrent at heights above 80 km. Aluminium, nickel and stainless steel produce relatively similar photocurrent below 60 km, as most of the Lyman-alpha photons are absorbed by the atmosphere and their photoelectric yields in the near-UV are relatively similar.

Figure 8 shows the expected photocurrent of a stainless steel electrode (\textit{i.e.} the base material of the MSPD) at an altitude of 85 km and for various inclination of the detector. As expected from its asymmetric design, the change of the photocurrent as a function of inclination is not straightforward due to the complex shadowing of the central electrode by the two concentric grids. In addition, the photocurrent can be seen to be much larger for the case at 90° compared to the other cases. This is most likely due to a perfect alignment of the two grids for this particular case, reducing the shadowing on the central electrode, and is expected to be less significant on the real detectors as both concentric grids are not as perfectly aligned together. Nevertheless, this is an important result as it confirmed the relationship between the recorded photocurrent and the instrument attitude, which could be used as an additional parameter to constrain the photocurrent from the MSP current during the analysis of the flight measurement.
Figure 6. Illumination on the MSPD for an inclination angle of (a) $0^\circ$, (b) $45^\circ$ and (c) $90^\circ$. Red shows the rays hitting the central electrode and blue the rays hitting the grids.
2.5 Comparison photocurrent measurements from a sounding rocket flight

Robertson et al. (2014) presented photocurrent measurements recorded by a 20 mm diameter aluminium plate onboard the CHAMPS sounding rocket. The rocket was launched from Andøya on October 13\textsuperscript{th} 2011 at 13:50 UT. The model was used to estimate the photocurrent emitted by such aluminium plate, using the solar spectral irradiance recorded by the SOLSTICE/SORCE instrument on this particular day and assuming an almost normal angle of incidence on the plate (\textit{i.e.} differences in angle of incidence from 0\textdegree{} to 30\textdegree{} can be considered negligible). Figure 9 shows the results of the calculation, compared to the measurements from Robertson et al. (2014) (see Figure 13 therein, here taken as the average of both the up-leg and down-leg measurements). Note that measurements below 700 nA/m\textsuperscript{2} and above 96 km were not provided by Robertson et al. (2014).
One can see that in the region of interest where MSP are expected, i.e. from 75 to 95 km, the decrease in photocurrent due to the Lyman-alpha absorption by molecular oxygen is reproduced by the model, although the scaling is quite different. The model underestimates the photocurrent above 90 km by a factor of five while slightly overestimating it below 80 km. The reason behind these differences was investigated, and the dependence on the atmospheric condition was confirmed to be negligible. Indeed, even an increase or a decrease of O$_2$ density by a factor of two would not significantly affect the resulting photocurrent. On the other hand, uncertainties on the photoelectric yield and reflectance used can have a much larger impact. As an example, the photoelectric yield of aluminium was slightly adjusted, increasing it by a factor of five around the Lyman-alpha wavelength while decreasing it by a factor of five for wavelengths above 180 nm. Such adjustments are not unrealistic considering the fact that the photoelectric yields used in the model were copied by hand from the log-scale figures presented in Feuerbacher and Fitton (1972), who did not include error bars on their measurements. The resulting photocurrent profile is shown in Figure 9.

One can see that the profile is much closer to experimental measurements from Robertson et al. (2014), although a factor of two difference still remains below 80 km. Correction for this difference would require an unrealistically low photoelectric yield at wavelengths above 180 nm. In addition, such slight adjustment of the photoelectric yield can also very nicely reproduce the trend seen by Robertson et al. (2014) but shifted about 2 km down. The difference in the photoelectric yield might also be due to contaminating material on the plate surface, as well as the purity and the surface roughness of the aluminium used. Considering the number of possible uncertainties, the base model was still able to reproduce the photocurrent within the same order of magnitude and with a similar absorption behaviour with respect to height.
3 Experimental measurement of the photocurrent

3.1 Overview of the experiment and apparatus

The experiment aims at using a known UV spectral flux to illuminate the detector and monitor the resulting photocurrent on the MSPD. Ideally, a calibrated UV light-source in a monochromator setup can provide a precise wavelength selection of the UV flux and allow for a detailed breakdown of the photocurrent as a function of the incident wavelength. However such configuration was not readily available and, for the purpose of keeping the cost low, narrow-band filters were used to select various UV wavelength-bands instead. Figure 10 shows the layout of the experiment. The experiment was conducted inside a 300 mm radius and 600 mm long vacuum chamber, to avoid absorption of the VUV light by the atmosphere.

The light-source used was an Heracles V01 Deuterium lamp which was calibrated by PTB (Physikalisch-Technische Bundesanstalt, the German national institute of metrology) back in 2011 for a previous calibration experiment (Ernst et al., 2011). Its normalized emission spectrum is shown in Figure 11a. Although the initial plan was to use four different filters centred around 121.5, 160, 200 and 250 nm to obtain the photocurrent in various passbands, no significant photocurrent was recorded when using the three latest filters. This was not due to lack of photons from the light-source in these spectral ranges but rather to the photoelectric yield of the material decreasing rapidly as the wavelength increases (see Figure 4), making the resulting photocurrent below the detection limit (∼10 pA). Hence, only the Lyman-alpha filter was used during the experiment and its transmission curve is shown in Figure 11b. Finally, the VUV flux from the light-source was monitored using a silicon photodiode mounted on a rotary stage in order to move it either in front or away from the light-source beam. Knowing the spectral response from the photodiode and the incident spectrum via the light-source spectrum and the filter transmittance, it is possible to estimate the photon flux emitted by the light-source from the photodiode current. However, the manufacturer only provided the spectral response of the diode down to 148 nm, and the response for lower wavelengths was unknown. Figure 11c shows the spectral response down to 148 nm, as well as two empirical response for wavelengths down to 115 nm. The first case represents a monotonic decrease of the spectral response as a function of wavelength whereas the second case represents an insensitivity of the photodiode to lower wavelengths. Pictures of the experimental setup are shown in Figure 12.
Figure 11. (a) Deuterium lamp spectrum measured by PTB. (b) Transmission curve of the Lyman-alpha filter. (c) Sensitivity of the photodiode, with the two different empirical cases below 148 nm.
Figure 12. (a) Deuterium lamp spectrum inside its PEEK holder. (b) Deuterium lamp covered with baffle and filter holder. (c) Setup inside the vacuum chamber, with MSPD in the background (0° inclination) and the photodiode on its rotating arm on the left.

3.2 Experimental measurements

Measurements were conducted for three different inclination angles of the MSPD: 0°, 45° and 90°. The initial plan was to record the photocurrent for additional inclination of the detector. However, large variations between multiple measurements taken at the same inclination were observed. These large variations were due to contamination on the Lyman-alpha filter, most likely caused by outgasing from the deuterium lamp socket, greatly degraded the VUV throughput over time as the light-source was operated under vacuum. An example is shown in Figure 13. One can notice the much larger decrease in the electrode current compared to the photodiode current. This suggests a larger absorption of the shorter wavelengths which are a larger contributor to the photocurrent but for which the photodiode is less sensitive. Note that a positive sign is adopted as convention for the electrode photocurrent, to be consistent with the calculation presented in Section 2.

To mitigate this issue, a rigorous cleaning of the filter using methanol was performed in between each measurement sequence taken at a given MSPD inclination. This effectively removed the contaminating material from its surface. The lamp MgF₂ window and the MSPD detector (inside an ultrasonic bath of ethanol) were also cleaned in between measurement sequences. The duration of each measurement sequence was kept below 15 minutes to minimize the time spent under vacuum and therefore limit the built-up of the contamination. Each measurement sequence was performed as follows: the light-source was turned on after reaching a pressure of 10⁻³ mbar and five minutes were allocated for its output light and current levels to stabilize. Then, a first recording of the electrode photocurrent was performed (each individual measurement consisted of 500 points recorded in about 1 min at a fixed bias using a Keithley 6430 sub-femtoamp remote sourcemeter). The photodiode was then placed in front of the beam and a recording of its current was performed. After that, a second measurement of the electrode photocurrent was performed, followed by a photocurrent measurement on each of the two grids, a second photodiode measurement, a third electrode photocurrent measurement and a final third photodiode measurement before switching off the light-source. Dark current measurements for the electrode, the two grids and the photodiode were also recorded with the light-source off and was around 10 pA for all surfaces. The biases used on the detector were the same as for one of the supposed flight configurations: central electrode grounded (in this case, to the chamber walls), inner grid at +6 V and outer grid at −6 V. Note that reaching a higher vacuum was not required for the purpose of the experiment, as the threshold for significant decrease in the photocurrent
Figure 13. Decrease of (a) the electrode photocurrent and (b) the photodiode current over time suggesting a degradation of the UV throughput due to contamination on the Lyman-alpha filter. Time starts at the start-up of the light-source. Red dash line shows a linear fitting.

due to absorption was observed to be around $10^{-2}$ mbar. Figure 14 shows the results for the 15 measurement sequences taken during the experiment in chronological order, five for each of the three orientations tested. The degradation of the throughput over time due to contamination is seen between the three measurements of the electrode photocurrent recorded on each sequence, even though the time spent under vacuum was less than 15 minutes. This added a large measurement uncertainty and for this reason, multiple measurement sequences were conducted for the same three inclination angles instead of measuring additional inclination angles. Moreover, a linear decrease on both the electrode photocurrent and the photodiode current can be seen between the different measurement sequences. This was interpreted as a residual contamination building up over time onto the filter surface, which could not be removed entirely by the methanol cleaning. Still, the cleaning was very effective as Figure 13 showed that the throughput would otherwise be decreased by two orders of magnitude after only 50 min of operation.

An estimation of the uncontaminated signal was made by removing the linear trend from the degradation. Table 1 shows the averaged corrected electrode photocurrent and corrected photodiode current for each of the three inclinations, with their corresponding 1-$\sigma$ errors calculated as the standard deviation of all fifteen measurements taken at a given inclination.
Figure 14. Results from the measurement sequences in chronological order for (a) the electrode photocurrent and (b) the photodiode current, for the three different inclinations.

Table 1. Average electrode photocurrent and photodiode current for each inclination.

<table>
<thead>
<tr>
<th>Inclination</th>
<th>Photodiode Current</th>
<th>Electrode Photocurrent</th>
</tr>
</thead>
<tbody>
<tr>
<td>0°</td>
<td>7.27 ± 0.12 nA</td>
<td>6.17 ± 0.39 nA</td>
</tr>
<tr>
<td>45°</td>
<td>7.45 ± 0.21 nA</td>
<td>6.34 ± 0.39 nA</td>
</tr>
<tr>
<td>90°</td>
<td>7.52 ± 0.32 nA</td>
<td>6.62 ± 0.42 nA</td>
</tr>
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3.3 Comparison with modelling

The photodiode currents from Table 1 can be used to determine the VUV flux from the light-source. This current is the result of the integral of the light-source spectrum multiplied by the filter spectral transmittance and the photodiode spectral sensitivity. By normalizing the light-source spectrum, one can use the recorded photodiode current to scale the light-source spectrum and determine the number of photons emitted by the light-source at each wavelength (assuming the light-source spectrum is constant and not a function of other parameters such as the temperature). As previously mentioned, an uncertainty remained on the photodiode sensitivity for wavelengths below 148 nm, and two empirical cases were considered: a monotonic decrease of the spectral response as a function of wavelength and an insensitivity to lower wavelengths (see Figure 11c). The resulting spectral flux of photons from the light-source can then be input into the photocurrent model from Section 2 to estimate the expected photocurrent. Table 2 shows the expected photocurrent determined from the above described calculation, compared to the measured photocurrent from Table 1. One can see that, depending on the case for the photodiode sensitivity, the estimated photocurrent is between three to eight times smaller than the measured one. This is comparable to the estimated photocurrent for the aluminium plate discussed in Section 2.5, which also underestimated the photocurrent by a factor from one to five. In addition, one can see that the predicted differences in photocurrent for the various inclinations is roughly similar to the error on the measured photocurrent, meaning that distinguishing between the different inclinations was unfortunately not possible based on the experimental measurements.

**Table 2.** Estimated electrode photocurrent based on the photodiode current from Table 1 compared to the experimentally measured electrode photocurrent, for each of the three inclination angles tested.

<table>
<thead>
<tr>
<th></th>
<th>Estimated electrode photocurrent (case 1)</th>
<th>Estimated electrode photocurrent (case 2)</th>
<th>Measured electrode photocurrent</th>
</tr>
</thead>
<tbody>
<tr>
<td>0°</td>
<td>0.81 ± 0.01 nA</td>
<td>1.85 ± 0.03 nA</td>
<td>6.17 ± 0.39 nA</td>
</tr>
<tr>
<td>45°</td>
<td>0.80 ± 0.02 nA</td>
<td>1.83 ± 0.05 nA</td>
<td>6.34 ± 0.39 nA</td>
</tr>
<tr>
<td>90°</td>
<td>1.00 ± 0.04 nA</td>
<td>2.32 ± 0.10 nA</td>
<td>6.62 ± 0.42 nA</td>
</tr>
</tbody>
</table>

4 Conclusion

The characterisation of the photocurrent induced by solar UV radiation is a crucial aspect of any plasma probe launched during day-time. A dual and complementary approach to the problem was presented by means of both modelling and experimental measurements in the particular case of a rocket-borne Meteor Smoke Particle Detector (MSPD) currently developed at the IAP.
The details of the photocurrent simulation were presented, including 1) an atmospheric absorption model providing the spectral flux of photons from 115 to 300 nm at any given height, 2) the material properties (photoelectric yield and reflectance) for various possible material and surface coatings of the detector, and 3) a detailed ray-tracing simulation providing a complete picture of the solar illumination onto the detector. The resulting photocurrent as a function of height was presented for the different material coatings of the MSPD. The model was also used to estimate the photocurrent on a circular aluminium plate and compared to actual photocurrent measurements by a similar plate made by Robertson et al. (2014), revealing an underestimation of the photocurrent by a factor one to five in the 75 to 95 km region. Investigating the reason of such difference revealed that the atmospheric parameters were not as critical as the material parameters for estimating the photocurrent, and it was shown that a moderate change in photoelectric yield could make the estimated photocurrent much closer to the measured one. On this topic, it is worth pointing out the lack of modern and reliable measurements of material properties, especially for the photoelectric yield, as all measurements used in this article were recorded more than forty years ago and retrieved from the published curves.

The MSPD photocurrent was also measured experimentally: a deuterium lamp was used to provide VUV light and a known passband was selected around the Lyman-alpha wavelength using a narrow-band filter. The light-source flux was monitored using a silicon photodiode and, knowing the light-source spectrum, the filter transmissivity and the photodiode sensitivity, an estimation of the spectral flux illuminating the detector could be made. Although the experiment had some issues, namely the contamination of the filter reducing which reduced transmissivity and the uncalibrated spectral response of the photodiode below 148 nm, some practical solutions were presented and an improved experiment could provide better results in the future. Based on the measured photon flux, the model was used to estimated the resulting photocurrent, which was then compared to the experimentally measured one. The model again underestimated the photocurrent by a factor from three to eight, depending on the photodiode sensitivity considered.

Precisely estimating the photocurrent is very challenging but the presented work revealed two important aspects which will be utilised to untangle the MSPD photocurrent from the actual MSP current. First, the photocurrent is affected by the detector inclination due to its asymmetric design, indicating a possible relation between the recorded photocurrent and the rocket attitude. Second, the model correctly predicted the decrease of the photocurrent due to O$_2$ absorption in the 75 to 95 km region of interest, given some scaling factors due to possible uncertainty on the photoelectric yield used. This effect is also expected during the flight and a relationship could be extracted based on the modelling, i.e. parametrization of the O$_2$ absorption with an adjusted photoelectric yield function, which could be used to fit the photocurrent as a function of height. This will be supported by the in-flight measurements of the O$_2$ density by the CONE instrument, also flying onboard the PMWE sounding rockets.

Appendix A: Realistic atmospheric curvature

The geometry of the atmosphere used in the model is shown in Figure A1, where $h$ is the height of a given point of interest $P$, $R$ is Earth radius, $\theta_z$ is the solar zenith angle, $x$ is the distance between $P$ and a given point $P'$ along the line-of-sight (LOS) and $h'$ is the corresponding height of the point $P'$. Using the law of cosine, one can express $h'$ as function of the distance.
\( x \) in a polynomial equation of order two. The path along the line-of-sight \( x \) is discretized with one kilometre steps, and the corresponding \( h' \) are calculated by solving the polynomial equation. The final light-path is obtained by considering values of \( h' \) between \( h \) and 240 km, the top of the atmosphere considered in the model.

![Figure A1. Geometry of the atmospheric curvature.](image)

**Acknowledgements.** The work was partially supported by the Swedish Government Agency for Innovation Systems (VINNOVA) contract no. 2016-04094. This work was supported by the German Space Agency (DLR) under grant 50OE1402 (project PMWE). The authors thank H.-J. Heckl and T. Köpnick for building the instrument.
References


