

1 **A portable dual smog chamber system for atmospheric aerosol field studies**

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9
10 **Abstract**

11 Smog chamber experiments using as a starting point ambient air can improve our understanding
12 of the evolution of atmospheric particulate matter at timescales longer than those achieved by
13 traditional laboratory experiments. These types of studies can take place under more realistic
14 environmental conditions addressing the interactions among multiple pollutants. The use of two
15 identical smog chambers, with the first serving as the baseline chamber and the second as the
16 perturbation chamber (in which addition or removal of pollutants, addition of oxidants, change in
17 the relative humidity, etc.), can facilitate the interpretation of the results in such inherently
18 complex experiments. The differences of the measurements in the two chambers can be used as
19 the basis for the analysis of the corresponding chemical or physical processes of ambient air.

20 A portable dual smog chamber system was developed using two identical pillow-shaped
21 smog chambers (1.5 m^3 each). The two chambers are surrounded by UV lamps in a hexagonal
22 arrangement yielding a total J_{NO_2} of 0.1 min^{-1} . The system can be easily disassembled and
23 transported enabling the study of various atmospheric environments. Moreover, it can be used
24 with natural sunlight. The results of test experiments using ambient air as starting point are
25 discussed as examples of applications of this system.

26
27 **1. Introduction**

28 Teflon reactors, known as smog or atmospheric simulation chambers have been valuable
29 research tools for the study of the complex chemical interactions that take place in the
30 atmosphere. Studies using such reactors date back to the 1950s (Finlayson and Pitts, 1976). The
31 use of these chambers eliminates many of the uncertainties resulting from the analysis of ambient

32 observations where several variables, such as weather conditions, pollutant emission rates,
33 dilution and transport are all contributing to the observed changes (Kim et al., 2009). Typically,
34 these reactors are made of Teflon, though there are some chambers that are made of metal or
35 glass (Cocker et al., 2001a; Paulsen et al., 2005; Kim et al., 2009). The volume of these
36 chambers varies from a few hundred liters up to hundreds of cubic meters, with the larger
37 configurations having lower surface to volume ratio, thus minimizing the wall effects (Cocker et
38 al., 2001a).

39 Chambers are placed either indoors or outdoors with the former having the advantage of a
40 well-controlled environment with constant temperature, light intensity etc. and the latter being
41 able to use natural sunlight (Laity, 1971; Jeffries et al., 1976; Leone et al., 1985; Carter et al.,
42 2005). For the indoor chambers, a variety of UV light sources can be used including black light
43 lamps (Laity, 1971), xenon, and argon arc lamps (Warren et al., 2008). The J_{NO_2} in indoor
44 atmospheric simulation chambers covers a wide range from zero (several metal chambers do not
45 have lights) to as much as around 1 min^{-1} (Kim et al., 2009). Some chamber facilities include two
46 identical smog chambers in order to use the first chamber as a reference (Kim et al., 2009). This
47 practice can enhance the quality of the results since numerous variables can have an effect on the
48 outcome of each experiment.

49 Different groups around the world have conducted thousands of smog chamber
50 experiments in order to simulate the behavior of pollutants in ambient air. These smog chambers
51 have been used to study, for example, secondary organic aerosol and its dependence on
52 temperature, relative humidity, UV intensity, NO_x levels, etc. (Halquist et al., 2009; Tritscher et
53 al., 2011). Other studies have focused on the characterization and evolution of primary emissions
54 from selected sources (Weitkamp et al., 2007; Kostenidou et al., 2013; Platt et al., 2013).

55 There have been a number of studies that used ambient air as the starting point of the
56 experiment. Roberts and Friedlander (1976) added SO_2 , 1-heptene and NO_x to a $96m^3$ outdoor
57 chamber filled with ambient air to study the aerosol formation. Heisler et al. (1977) used ambient
58 air to fill an outdoor $80 m^3$ Teflon chamber to study the growth rate of the particles. Pitt et al.
59 (1977) concluded that the addition of N,N'-diethylhydroxylamine in ambient air enhances the
60 formation of ozone, peroxyacetyl nitrate, and light-scattering particles. Kelly (1987) used a 0.5
61 m^3 chamber to investigate the HNO_3 formation in ambient air. Kelly and Gunst (1990) studied
62 the ozone dependence on hydrocarbons and nitrogen oxide using ambient air. Lee et al. (2010)

63 investigated the correlations between light intensity and ozone formation for ambient air in
64 Seoul. The potential OA enhancement or sink due to aging of ambient air has been also studied
65 in the field by the use of oxidation flow reactors (OFR) in various ambient environments (Tkacik
66 et al., 2014; Ortega et al., 2016). The OFR uses high OH levels, thus simulating atmospheric
67 oxidation in timescales of several days to weeks. On the other hand, typical experiments in
68 atmospheric simulation chambers take place at close to ambient OH levels and simulate hours to
69 a few days of aging.

70 There have been a few efforts to use portable smog chamber facilities for different
71 applications. For example, Shibuya et al. (1981) used a portable 4.5 m³ smog chamber, installed
72 in a vehicle, to study the ozone formation in ambient air. Hennigan et al. (2011) and Stockwell et
73 al. (2014) developed portable twin-chamber systems with UV lights to monitor the aging of
74 combustion emissions. A portable smog chamber facility was also developed by Platt et al.
75 (2013) featuring a 9 m³ Teflon reactor that can be mounted on a trailer.

76 The interactions of the walls of the chamber with the pollutants inside it represent a major
77 experimental challenge and have been the topic of several studies. Gas-phase pollutants (e.g.,
78 ozone) are lost to the walls and increased relative humidity tends to increase the decay rates
79 measured (Akimoto et al., 1979). The walls also can serve as a source of OH mainly outgassing
80 nitrous acid (HONO) (Jeffries et al., 1976; Akimoto et al., 1979; Carter et al., 1982; Sakamaki et
81 al., 1983; Pitts et al., 1984; Jenkin et al., 1987; Glasson and Dunker, 1989; Killus and Whitten,
82 1990; Finlayson-Pitts et al., 2003). In most cases OH production increases with temperature,
83 humidity and NO₂ concentration (Sakamaki et al., 1983; Pitts et al., 1984; Kleffmann et al., 1998;
84 Svensson et al., 1987; Jenkin et al., 1987). Akimoto et al. (1987) and Sakamaki and Akimoto
85 (1988) reported higher HONO concentrations at higher light intensity. Auxiliary mechanisms
86 have been developed to describe the background reactivity of smog chambers (Bloss et al., 2005;
87 Carter et al., 2005; Hynes et al., 2005; Rohrer et al., 2005; Metzger et al., 2008; Wang et al.,
88 2011; Wang et al., 2014). In these mechanisms, the role of the chamber walls as sinks and
89 sources of gas-phase pollutants is parameterized and these reactions are added to the actual gas-
90 phase chemistry model used to interpret the measurements in the chamber.

91 Typically, smog chamber experiments isolate a pollutant or a mixture of pollutants
92 emitted by a source and focus on its chemistry. In most cases, clean air is used as the starting
93 point of the experiment. While the corresponding results are clearly valuable, these experiments

94 might miss the potentially important interactions of the examined chemical system with other
95 pollutants existing in ambient air. To close this major gap between the laboratory studies and the
96 ambient atmosphere, a portable dual smog chamber system with UV lights is designed and tested
97 in this study. The chamber has been developed to use ambient air rather than clean air as its
98 starting point. Having the advantage of being portable enhances the opportunities to study
99 several environmental scenarios and simulate the processes occurring in previously out-of-reach
100 chemical regimes (e.g., very aged air masses). The preliminary tests of the operation of this
101 system are presented.

102

103 **2. Design of the dual smog chamber system**

104 **2.1 Smog chambers**

105 Relatively small Teflon reactors were selected for this system so that they can be filled in a
106 matter of minutes, while having a volume adequate to support a 4-hourbatch experiment, losing
107 less than a third of their volume based on the standard instrumentation sampling flow rates. A set
108 of two identical smog chambers was constructed from Teflon (PTFE) film (DuPont PTFE 2 mil,
109 0.5 m wide.). Each chamber has a nominal volume of 1.5 m³. The two chambers are pillow-
110 shaped and are permanently mounted on a metal frames (Figure 1a). The relatively small volume
111 of the chambers along with the fixed frame enables their easy and safe transport without having
112 to disassemble them or to remove the sampling ports. Relative humidity (RH) and temperature
113 sensors are also fixed on the chambers. The frame dimensions are 1.7 x 0.5 x 1.7 m. Two
114 sampling ports (one per chamber) with multiple lines and a temperature/RH sensor were installed
115 on the reactors.

116 We constructed the chambers in our laboratory in Patras. The reactors were thoroughly
117 cleaned and conditioned before the first characterization experiment. The cleaning procedure
118 involved first introduction of high O₃ concentrations with the UV lights on and heating to
119 approximately 50 °C. Clean air was passed then through chambers for several hours. Blank
120 experiments were performed periodically both in the lab (during the characterization phase) and
121 in the field. The particle wall losses are measured after each field experiment. We did not
122 observe any evolution of the wall chemical behavior in these initial tests.

123 Sampling is alternated between the two chambers every three minutes by an automated
124 three-way valve synchronized with the operation of the corresponding instrumentation. This

125 allows a total duration of the experiments of more than 4 hours without the addition of make-up
126 air. In order to eliminate interferences and memory effects due to this periodical alteration of the
127 sampling lines, adequate time (30 s) is allowed within the three-minute sampling cycle for the
128 lines to be flushed with the sample air from the next chamber. This is achieved by synchronizing
129 the line flushing with the measuring instrumentation and discarding the data collected during this
130 30 s period.

131

132 **2.2 Portable UV lighting system**

133 A hemispheric design was selected with sixty 36 W UV light lamps (Osram, L36W/73) in a
134 hexagonal arrangement. The lamps were mounted on five metal frames (12 per frame) creating
135 five sub-structures (Figure 1b) that can be easily disassembled and transported. Once assembled
136 the UV light support structure had a footprint of 4.5 x 4.5 m and a height of 2.5 m. Figure 1b
137 shows the UV light assembly without the covering material. Flexible tent poles were used to
138 create a dome that can be partially or fully covered protecting the chambers from the weather
139 elements (Figures 1c and 1d). The sixth side does not include lights and is used as an entrance
140 for chamber maintenance. The lights can be remotely operated at 20, 40, 60, 80 and 100% levels.
141 The light fixtures include aluminum mirrors in order to direct the light towards the center of the
142 dome, thus maximizing the light intensity delivered to the chambers. When all lights are on, the
143 corresponding J_{NO_2} is 0.1 min^{-1} . The spectrum of the lights peaks in the 350-400 nm region (SI
144 Figure S1). The two chambers are placed inside this dome having at least a 0.5 m clearance from
145 the UV lights when full. This design also allows the use of a single 10 m³ chamber if so desired.

146

147 **2.3 Subsystems**

148 A dual-head metal bellows pump (model MB-602) is used to fill the chambers with ambient air
149 delivering 80 L min^{-1} per pump head. Both chambers can be filled in around 20 min. Manual
150 two-way valves were installed prior to the chamber inlets for isolation and selective filling
151 purposes. Prior to any experiment with ambient air, both chambers are flushed with ambient air
152 with the metal bellows pump until the NO_x and O₃ levels matched the ambient concentrations.
153 To ensure chamber similarity the chambers are used alternatively in experiments as a
154 perturbation/reference chamber.

If required clean particle free air can be introduced in the chambers. Dry air is generated by an oil-less compressor (Bambi VT200D) and further purified by activated carbon (Carbon cap, Whatman), HEPA filters (HEPA capsule, Pall) and silica gel (Silica gel rubin, Sigma-Aldrich). The compressor and air cleaning system are not used for the actual experiments. In these experiments the chambers are filled with ambient air without the use of cleaning devices. The compressor/cleaning system is used for the cleaning of the chambers between experiments and for blank or other chamber characterization experiments. Typically, the concentrations of ozone, NO_x and larger VOCs are below or close to the detection limit in the chambers when they are filled with clean air from our system. The scrubbers were replaced regularly and the residence time inside them was kept as high as possible (maintaining the corresponding flow rates as low as possible). The concentrations of some of the small oxygenated VOCs such as acetone, acetic acid and methanol were slightly elevated compared to the cylinder zero air.

A subunit including the above systems (except for the filling pump and the compressor) was added to one of the metal frames of the system. This subunit also includes a syringe pump, an atomizer (TSI model 3076) and a silica gel diffusion drier (Silica gel rubin, Sigma-Aldrich) for seed generation. Additionally, a bubbler subsystem for HONO introduction and an ozone generator (Azcozon, model HTU-500) were used. The concentration of OH when HONO was added was estimated in all experiments by the decay of d-butanol over time. The estimated levels of added HONO were of the order of 100 ppb. Two temperature/RH sensors (Omega, model RH-usb) and a personal computer with Labview control for the sampling selection valve are also part of this system.

176

177 **2.4 Instrumentation**

The set of instruments selected for the use with the chamber system include: aHR-ToF-AMS (Aerodyne Research Inc.), a PTR-MS (Ionicon Analytik), a Scanning Mobility Particle Sizer (SMPS, classifier model 3080, DMA model 3081, CPC model 3787, TSI), an ozone monitor (API Teledyne, model 400E) and a NO_x monitor (API Teledyne, model T201). These instruments are located inside the FORTH mobile laboratory (Fig 1c) next to the chambers. Details on the instrumentation used can be found elsewhere (Kostenidou et al., 2013; Kaltsonoudis et al., 2016). With this configuration, a total sampling flow rate of 2.5-3 L min⁻¹ is used that removes less than 0.1 m³ from each chamber per hour.

186

187 **2.5 Experimental procedure**

188 The instrumentation is first used to characterize the ambient conditions for at least a couple of
189 hours. After filling of the chambers is completed, sampling is switched from ambient
190 measurements to the chambers and an initial characterization of the sampled air inside the
191 chambers takes place. Then a perturbation (addition of oxidant or pollutant) is implemented in
192 one of the chambers, while the other is used as a reference. Following the completion of the
193 experiment ammonium sulfate seeds are introduced into both chambers to measure their loss rate
194 on the walls over time. In this step, the chambers may be refilled with particle free air. This last
195 stage is used to quantify the particle size-dependent wall loss rate constants in order to make
196 corrections to the rest of the measurements. Finally, the instrumentation is switched back to
197 ambient observations and the chambers are flushed with either ambient air and /or clean air in
198 preparation for the next experiment.

199

200 **3. System evaluation**

201 The system was developed and evaluated in Patras, Greece and also during the Finokalia Aerosol
202 Measurement Experiment (FAME 16) campaign. Finokalia is a remote site in Crete, Greece
203 (Kouvarakis et al., 2000). The field campaign took place during May-June 2016. Additional tests
204 aimed on improving the performance of the setup were performed indoors at Carnegie Mellon
205 University in Pittsburgh, United States. The present work is based on the results of 51 chamber
206 characterization experiments and 7 field test experiments. The characterization experiments
207 include 15 blank or contamination related experiments, 14 experiments characterizing wall
208 losses, 6 experiments quantifying the ambient air sampling efficiency, 3 experiments for the
209 measurement of J_{NO_2} , 9 experiments related to RH and UV variations, and 4 VOC loss
210 experiments. The list of these experiments and some additional information can be found in
211 Table S1 in the Supplementary Information.

212

213 **3.1 Contamination tests**

214 Tests were conducted in the field in order to assess the potential contamination of the chambers
215 by ambient air. The chambers were filled with clean (particle free) air and the particle
216 concentration inside the chambers was monitored by an SMPS. Figure 2 shows the total number

217 concentrations in the two chambers. The particle number concentrations remained below 10 cm^{-3}
218 in both chambers for several hours. The aerosol mass concentration (not shown) was less than
219 $0.01\text{ }\mu\text{g m}^{-3}$. This suggests that clean conditions can be maintained for both chambers for the
220 duration of a typical field experiment.

221

222 **3.2 Chamber similarity**

223 Similar results should be obtained when identical experiments take place in the two chambers in
224 order to safely use one of them as reference. To establish this, ambient air was introduced in both
225 chambers and the evolution of the concentrations and composition of the particulate matter and
226 gas pollutants was measured. An SMPS measured the size distribution and an AMS the
227 particulate composition. The measured chamber and ambient mass concentrations (Figure 3a)
228 and the AMS spectra (Figures 3c and d) were in good agreement between the two chambers and
229 the ambient. The particle mass concentration in the chambers was approximately 85% of the
230 ambient levels. The theta angle (Kostenidou et al., 2009) between the organic aerosol spectra in
231 the two chambers and the ambient air was in the range of 2.5-6 degrees, suggesting that identical
232 results can be obtained when filling these chambers with ambient air and that the filling process
233 does not contaminate the air sample. The theta angle is a measure of the similarity of the OA
234 spectra (similar to the often used R^2). Each mass spectrum is treated as a vector (each m/z is an
235 element of the vector) and theta is the angle between two such vectors. We prefer to use theta
236 angle for AMS spectra comparisons because it can distinguish better small differences in spectra
237 than the coefficient of determination cannot.

238 Pump and tubing losses during the filling procedure were evaluated in order to establish
239 the difference between ambient concentrations and the ones obtained in the chambers. The same
240 number distributions are achieved in both chambers after filling them with ambient air. The
241 penetration efficiency through the tubing and the pump for particles with diameter larger than
242 80nm is close to 100%, while for smaller particles due to higher diffusional deposition the
243 penetration efficiency is 45%. The length of the tubing is approximately one meter (with a 0.5 in
244 diameter). The estimated losses for this tube for the flow rates used and for particles in the 20-80
245 nm size range are 1-3 percent. Therefore, most of the losses are occurring in the pump.
246

247

248 **3.3 Particle wall losses**

249 Loss of particles to the walls is one of the processes that complicate the analysis of smog
250 chamber experiments. The use of smaller reactors with lower surface to volume ratios can
251 accelerate these losses. Disturbances of the Teflon reactors tend to increase the wall loss rates
252 due to the buildup of static charges on the chamber walls. Transporting and installing the reactors
253 also results in higher wall loss rate constants (Wang et al., 2018).

254 In order to assess the wall loss behavior of the system experiments were conducted both
255 in the laboratory and in the field. In all cases, ammonium sulfate seeds were added to the
256 chambers and their decay with time was measured. Typically, the chambers were first filled with
257 clean (particle free) air and then ammonium sulfate seeds were introduced. A solution of 5 g L^{-1}
258 ammonium sulfate was used for the atomizer and a flow rate of 2 L min^{-1} . The decay of the
259 particles was monitored by an SMPS. Size dependent wall loss rate constants were calculated
260 correcting for coagulation (Wang et al., 2018). Figure 4a represents the average size dependent
261 profiles for the loss rate constant K_c of the two chambers for the laboratory experiments. On the
262 field, higher rate loss constants were measured (Figure 4b). For example, loss rate constants of
263 0.2 h^{-1} were measured for the 350 nm particles in the lab, while for the same size range, a value
264 of approximately 0.5 h^{-1} was measured in the field. Figure 4c and 4d show the wall loss profiles
265 of the two chambers when deployed in the Finokalia campaign over three days of measurements.
266 In both chambers the wall loss rate constants were decreasing over time. During the field
267 deployment of the chambers their handling and the corresponding induced friction resulted in
268 higher charges on the chambers walls and thus higher particle wall losses. These higher losses
269 had also a stronger size dependence. On the other hand, when the chambers were inside the lab,
270 there was no build-up of charges and the losses were lower and less size-dependent. A detailed
271 analysis of the losses of particles in Teflon chambers (both in the laboratory and the field) has
272 been presented by Wang et al. (2018). For this reason, the particle wall loss rates are measured
273 after each experiment, by the addition of ammonium sulfate seeds. The chambers in the
274 laboratory underwent minimum handling during each experiment and thus achieved low loss rate
275 constants for a wide range of particle sizes.

276 In order to assess if it is possible to minimize such charges a test was conducted in the
277 Teflon reactors in the lab. The chambers were moved in a different location inside the building
278 where the lab is located. The two reactors were handled in exactly the same way simulating the

279 handling during a field deployment. One of the chambers was inflated with air to almost half-full
280 while the other was empty. The particle wall-losses were measured before and after the
281 movement. Figure 5 represents the loss rate constants in the two chambers because of the
282 movement. The loss rate did not change in the partially inflated chamber. The other chamber
283 though experienced an increase in the loss rate constants, almost doubling for the particles in the
284 range 50-200 nm, due to stronger friction of the Teflon walls with each other and thus building
285 static charge. No significant change was noticed for particle larger than 250 nm.

286 The high particle wall losses introduce uncertainty in the results, because the wall-loss
287 corrections dominate the corrected concentration values. If the losses are very high, the
288 maximum duration of such experiments may be limited. We have been working on developing
289 methods to minimize these effects. Moving the chambers to the field site either fully or at least
290 partially inflated inside our mobile laboratory clearly helps.

291

292 **3.4 VOC concentrations**

293 Concentrations of the VOCs measured by the PTR-MS were within a few percent of their
294 ambient levels. In most cases, no noticeable differences were seen. Tests indicated that there was
295 no detectable contamination due to the metal bellows pump during the filling process of the two
296 chambers. Vapor loss experiments were also performed for a few selected VOCs. The measured
297 wall loss rates were quite low (less than 1 percent per hour) for toluene and a-pinene. Their
298 concentrations remained for all practical purposes stable during the experiment.

299

300 **3.5 NO_x, O₃, and OH interactions with the walls**

301 A series of experiments were performed to quantify the loss rates of NO_x and O₃ to the Teflon
302 walls of the chambers and the OH production rates. These can be used for the development of an
303 auxiliary mechanism. The experiments were carried out for two light intensities (J_{NO_2} of 0.03
304 min⁻¹ and 0.1 min⁻¹) and for two RH values (RH<10% and 50±15%). The OH levels in the
305 chamber were estimated based on the decay of d-butanol. HONO off-gassing from the chamber
306 walls was not measured directly, but was estimated based on the OH levels. Effective OH
307 production rates were estimated using a pseudo-steady-state assumption. The OH production
308 rates were practically negligible at low RH, but increased at 50% RH and depended on light
309 intensity. The results of these measurements can be found in the SI. These measurements

310 indicate that the HONO injections were the dominant source of OH in our perturbation
311 experiments. However, the contribution of the walls can be non-negligible under some
312 conditions for the baseline chamber. To minimize complications, d-butanol was injected in all
313 experiments allowing the direct estimation of the OH concentration in both chambers. As a result
314 the reported OH exposure takes into account the wall sources as well.

315

316 **4. Laboratory testing**

317 The performance of the system was tested in experiments that took place indoors at Carnegie
318 Mellon University (Center for Atmospheric Particle Studies). The potential aging of urban
319 background air masses in Pittsburgh, PA, by OH radicals was used as a pilot study for the system
320 evaluation. Fewer UV lights were used in this test resulting in a J_{NO_2} equal to 0.03 min^{-1} .

321

322 **4.1 Experimental procedure**

323 Prior to the experiment, both chambers were flushed with particle-free air overnight under UV
324 illumination to remove any residual particles and gas-phase organics. Both chambers were filled
325 with ambient air using the metal bellows pump. During the filling procedure, the instruments
326 were measuring ambient conditions. After the addition of ambient air in the chambers, d9-
327 butanol (60 ppb) was added to both of them as an OH tracer (Barment et al., 2012). The OH
328 levels can be estimated by the decay in the d9-butanol concentration measured by the PTR-MS
329 system at m/z 66. The reaction constant for the butanol reaction with OH is $3.4 \times 10^{12} \text{ cm}^3$
330 molecules $^{-1} \text{ s}^{-1}$. HONO was injected only into the perturbation chamber for about 3 min to
331 produce OH upon UV illumination. The UV lights then turned on were illuminating both
332 chambers. After the completion of the perturbation experiment, a seed wall-loss experiment was
333 conducted to quantify the particle wall-loss rate constants for the two chambers as described in
334 section 3.3.

335

336 **4.2 Results and discussion**

337 The wall-loss corrected total particle number concentration as measured by the SMPS is
338 shown in Figure 6. The instruments were measuring ambient conditions during the filling
339 process. The average ambient number concentration was around 2500 cm^{-3} . HONO was injected
340 in the perturbed chamber at $t=0.4 \text{ h}$. After turning on the UV lights ($t=0.6 \text{ h}$) an increase in the

341 total particle number and volume in the perturbed chamber was observed while no change in the
342 control chamber was noticed. The increase in the perturbed chamber is due to the formation of
343 new particles (Figure 7).

344 Based on the AMS measurements, the ambient air used to fill the chambers contained on
345 average $3.6 \mu\text{g m}^{-3}$ of non-refractory PM₁ with organics accounting for 75%, sulfate 17%,
346 ammonium 6% and nitrate 2%. The collection efficiency of the AMS measurements was found
347 to be 0.6 based on the algorithm of Kostenidou et al. (2007), while the estimated OA density was
348 1.2 g cm^{-3} . The calculated theta angle (Kostenidou et al., 2009) between the ambient and the
349 chamber organic mass spectra vectors was around 5 degrees, indicating that the aerosol
350 composition inside the chamber was essentially the same as in the ambient.

351 To quantify the secondary aerosol formation, data were corrected for both the collection
352 efficiency and for particle wall-losses. Figure 8 shows the concentrations of the major PM₁
353 components in the two chambers. An increase of concentration was observed in the perturbed
354 chamber. After 2.5 hours of exposure to OH an additional $1.5 \mu\text{g m}^{-3}$ of organics, $0.2 \mu\text{g m}^{-3}$ of
355 sulfates, $0.1 \mu\text{g m}^{-3}$ of nitrates and $0.1 \mu\text{g m}^{-3}$ of ammonium was formed. The average OH
356 concentration in the perturbed chambers was $8.0 \times 10^6 \text{ molecules cm}^{-3}$ corresponding to
357 approximately 11 h of equivalent exposure to an ambient OH = $1.5 \times 10^6 \text{ molecules cm}^{-3}$. The OH
358 concentration in the control chamber was an order of magnitude less $8 \times 10^5 \text{ molecules cm}^{-3}$. The
359 organic spectra of the additional formed SOA and the initial OA in the perturbed chamber were
360 relatively similar; their theta angle was 10 degrees (Figure 9). The mass spectrum of the
361 processed OA characterized by lower fractional contributions at m/z 43 and 44.

362 The evolution of the oxygen to carbon ratio of the organic aerosol in the two chambers is
363 shown in Figure 10. The O:C of the ambient organic aerosol and of the initial OA in the two
364 chambers was 0.44. After the OH introduction and the SOA production in the perturbed
365 chamber, the O:C decreased slightly to 0.40. The O:C in the control chamber remained
366 approximately the same. The decrease of the O:C in the perturbed chamber indicates that the
367 additional formed SOA had smaller O:C than the ambient. The average O:C ratio in other
368 ambient experiments conducted in Pittsburgh was around 0.5 indicating an already moderately
369 oxidized aerosol population. For comparison, the average O:C ratio in the FAME 2008 and
370 FAME 2009 campaigns was 0.8 and 0.5, respectively (Hildebrandt et al., 2010). The results of

371 such ambient air experiments with detailed analysis of the formed aerosol, comparison with
372 ambient and laboratory measurements are included in a forthcoming publication.

373

374 **5. Conclusions**

375 A portable dual chamber system has been developed for field studies using ambient air as
376 a starting point. The system has been evaluated and no contamination was observed during a
377 typical experiment. The concentration in the two chambers when filled with ambient air are
378 within a few percent of each other. Particle losses during filling were less than 20%. No
379 noticeable losses or cross-contamination was observed for the measured VOC species.

380 Higher wall loss rates were observed when the chambers were deployed in the field,
381 compared to the lower and stable rates observed when the chambers were inside the laboratory,
382 due to higher electrostatic charges induced during their movement. A reduction in the wall loss
383 rates was observed when the chambers are deployed in the field, suggesting that they should be
384 measured after each experiment. The losses can be reduced if the chambers are transported
385 partially inflated. Initial laboratory experiments show promising results in respect to potential
386 aging properties of urban background air in Pittsburgh. An additional $1.5 \mu\text{g m}^{-3}$ of SOA was
387 formed after 12 h of equivalent OH exposure with a moderate decrease of the O:C ratio.
388 Implementing the system in the field will enable the study of complex systems that were
389 previously out of reach with traditional stationary chamber facilities.

390

391 *Data availability.* The data in the study are available from the authors upon request
392 (spyros@chemeng.upatras.gr).

393

394 *Author contributions.* CK constructed the facility, participated in the experiments and wrote the
395 paper. SJ conducted and analysed the wall loss and test experiments and contributed to the
396 writing of the paper. EL and KF helped in the construction of the facility and assisted in the
397 experiments. SNP was responsible for the design of the study, the synthesis of the results and
398 contributed to the writing of the paper.

399

400 *Competing interests.* The authors declare that they have no conflict of interest.

401

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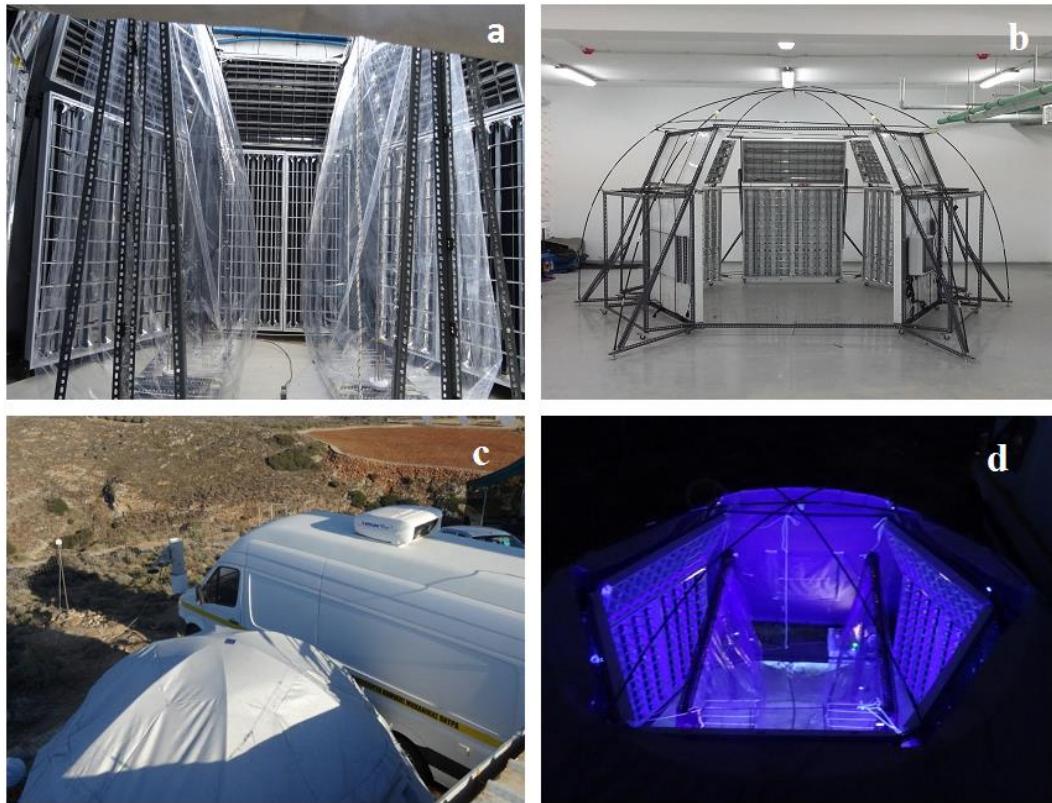
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580 **Figure 1.** Pictures of the portable dual chamber system: a) the dual chambers; b) UV light
581 assembly; c) field deployment during the FAME 16 study; d) system configuration with the UV
582 lights on and the top cover open.

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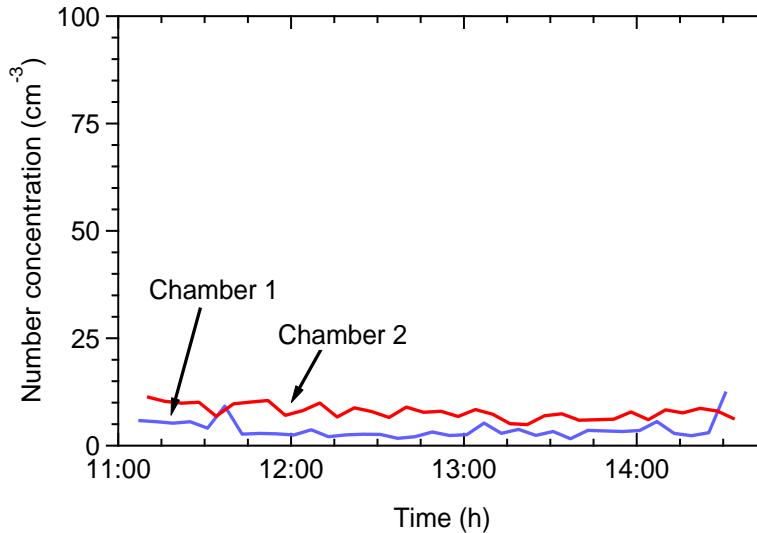
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593 **Figure 2.** Total particle number concentrations as a function of time when the chambers were
594 filled with clear air in the field for leak check of the chambers.

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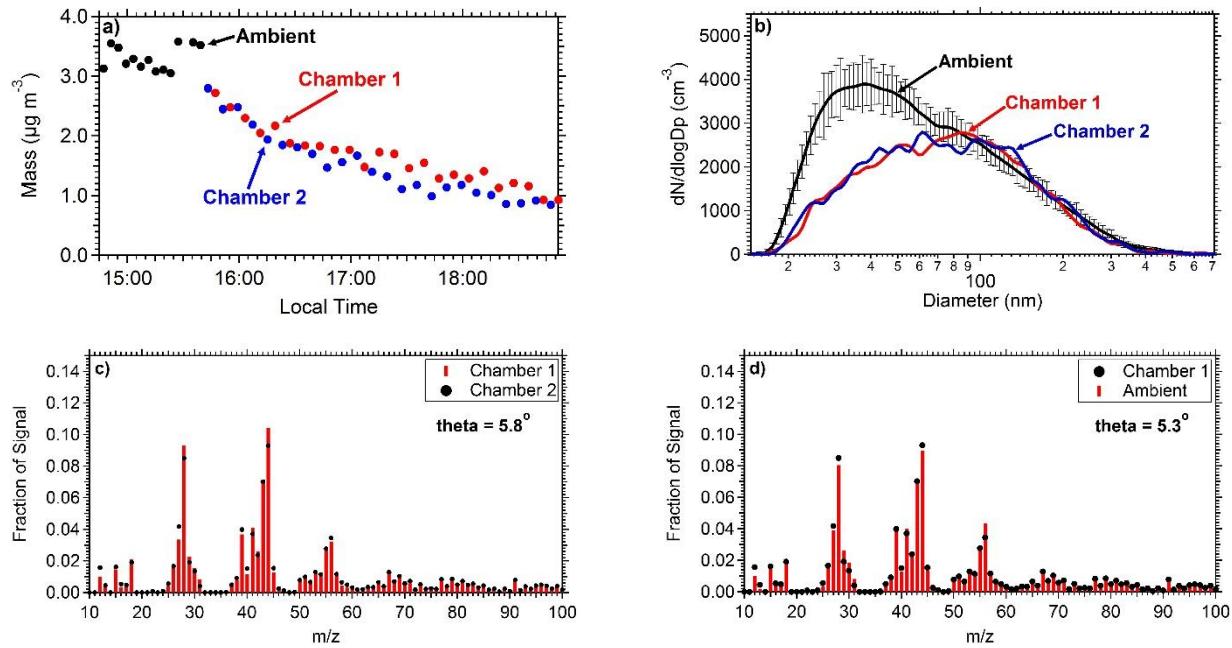
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609 **Figure 3.** Comparison of the measurements between the two chambers and between ambient
 610 measurements: a) Mass concentration ($\text{PM}_{0.7}$) as measured by the SMPS in both the chambers
 611 and the ambient. b) Number distributions inside the chambers and in the ambient (the error bar
 612 represent one standard deviation). c) Average aerosol mass spectra of chamber 1 and chamber 2
 613 filled with ambient air. d) Average aerosol mass spectra of ambient air and chamber 1.

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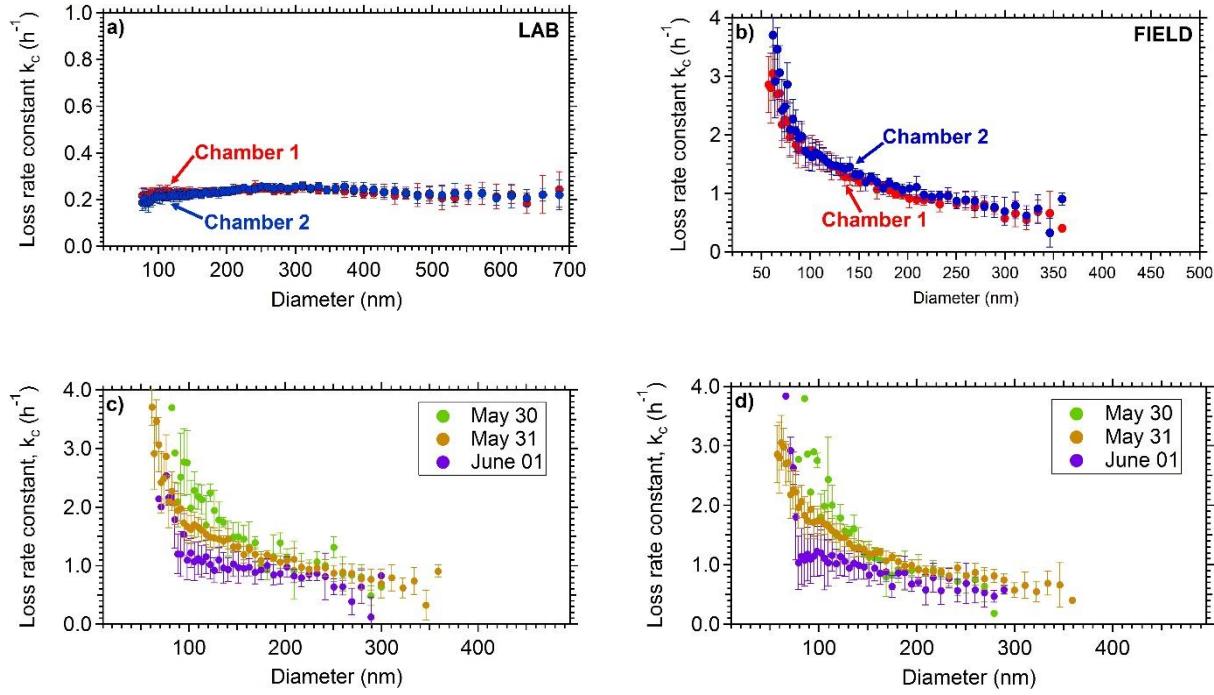
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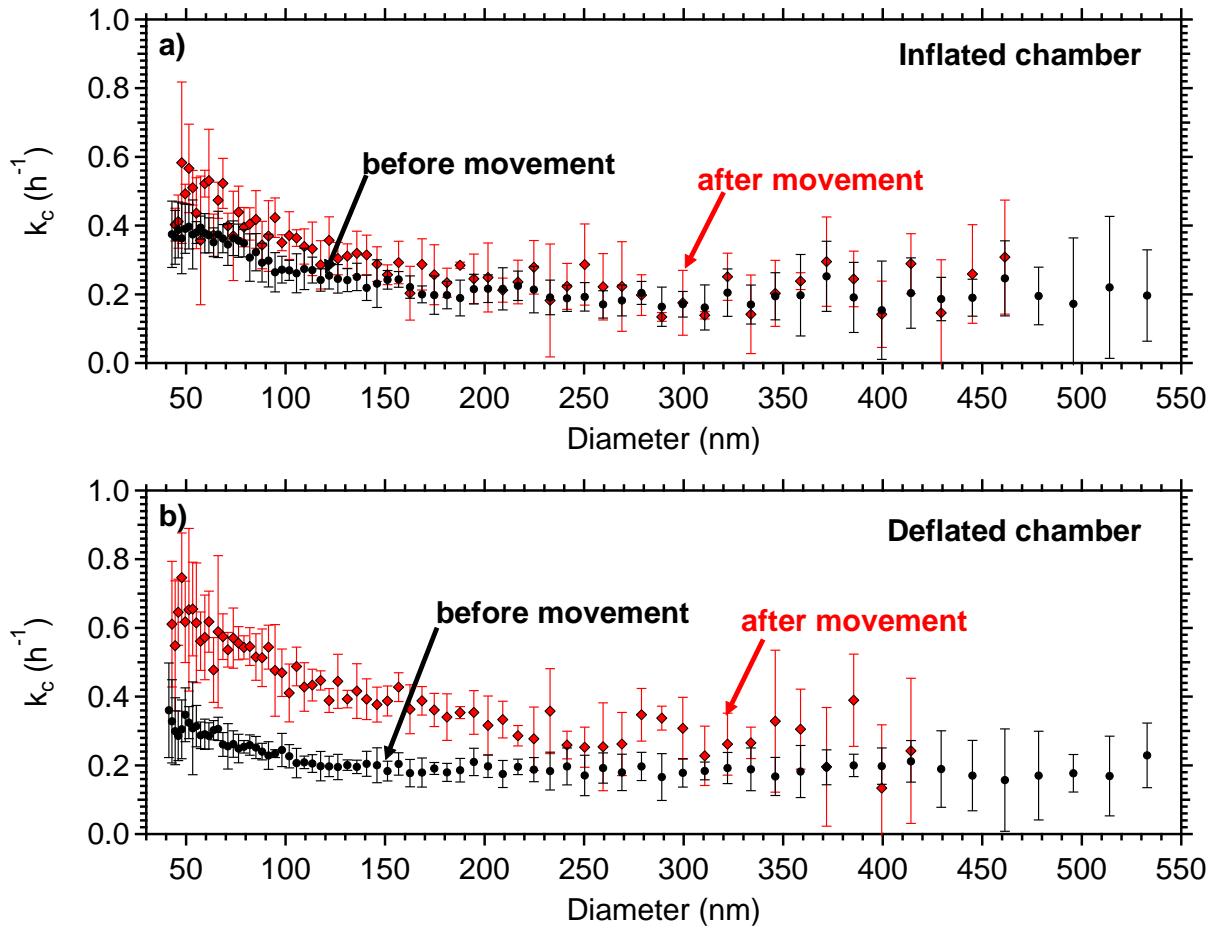
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620 **Figure 4.** Coagulation-corrected particle wall-loss rate constant as a function of particle size for
621 the two chamber a) in the laboratory and b) in the field. The particle wall-loss rate constant as a
622 function of particle size during three consecutive days for the field deployment. Figure c
623 corresponds to chamber 1 and d) to chamber 2.

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632 **Figure 5.** Coagulation-corrected particle wall-loss rate constant as a function of particle size for
 633 the two chamber after the movement a) in the partially inflated chamber and b) in the deflated
 634 chamber. The error bars represent one standard deviation.

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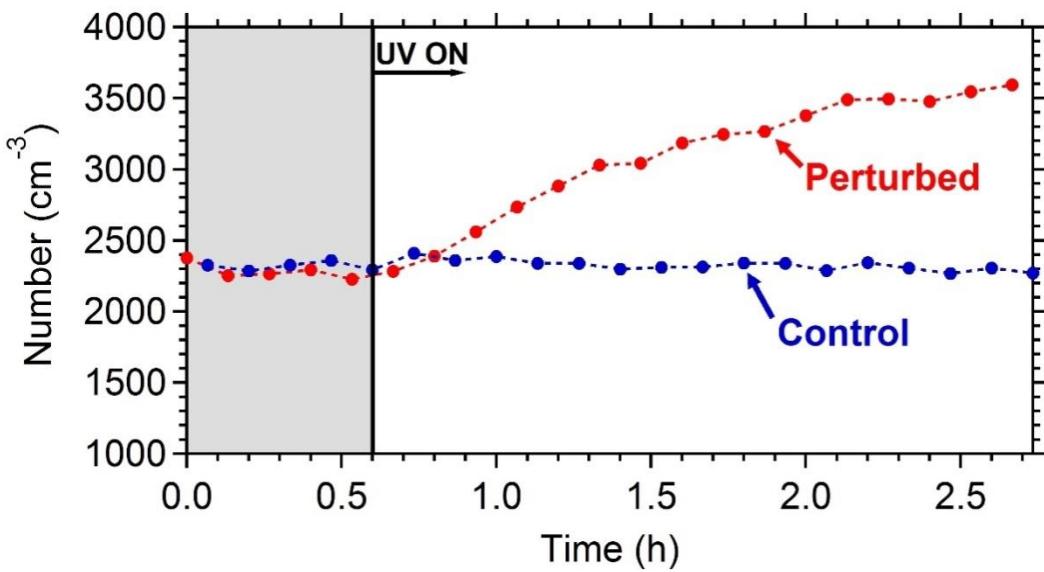
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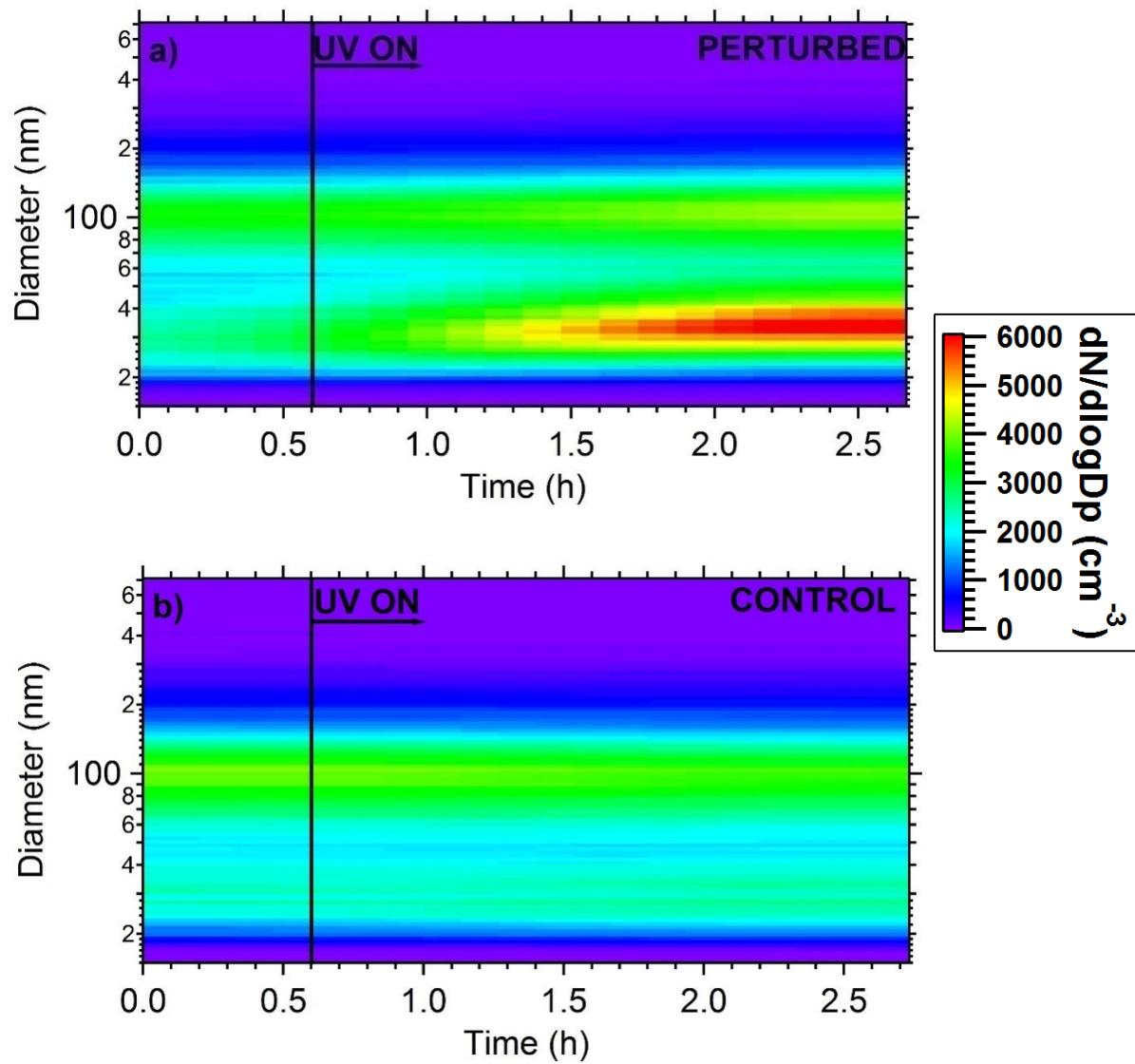
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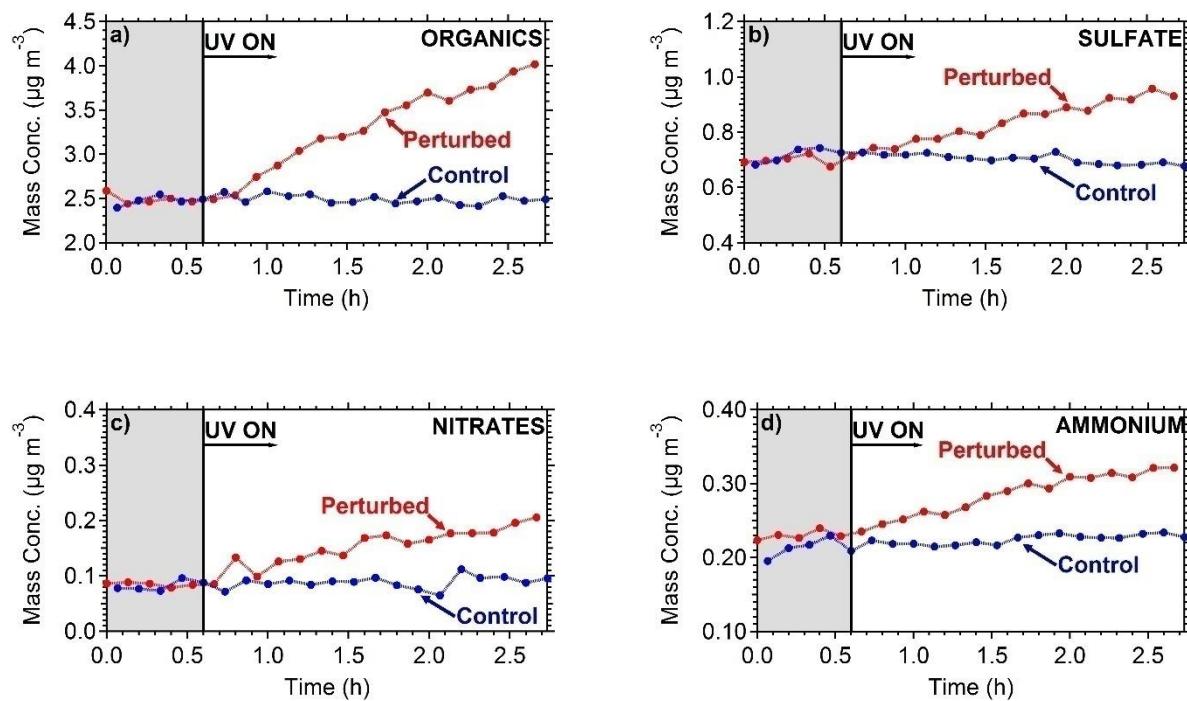
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646 **Figure 6.** The wall-loss corrected SMPS-measured aerosol number concentration. HONO was
647 added only in the perturbed chamber at $t=0.4$ h to produce OH under UV illumination. The
648 shaded area indicates that the chambers were dark.
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668 **Figure 7.** Plots of the evolution of particle number distributions during the HONO perturbation
669 experiment in Pittsburgh. (a) Perturbed chamber and (b) Control chamber.
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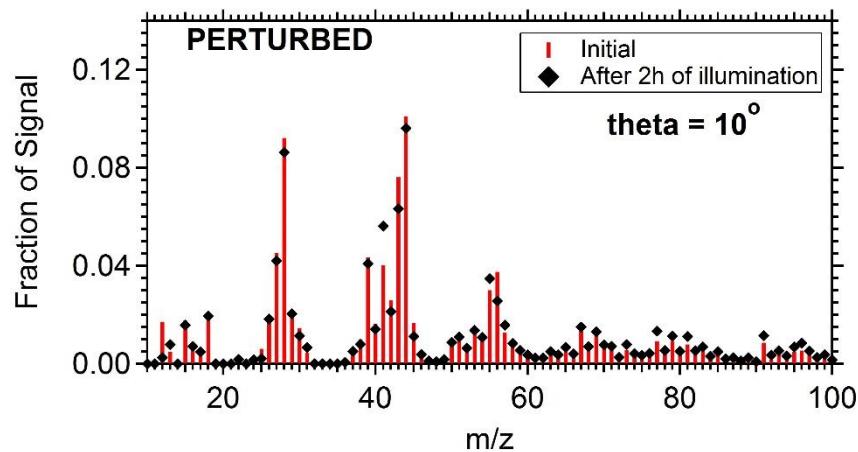
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677 **Figure 8.** The particle wall-loss corrected concentrations of the major PM₁ components
678 measured by the AMS a) organics, b) sulfate, c) nitrates and d) ammonium. The shaded area
679 indicates that the chambers were dark. Data have been corrected for the collection efficiency
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700 **Figure 9.** The organic mass spectra after filling and after two hours of UV illumination in the
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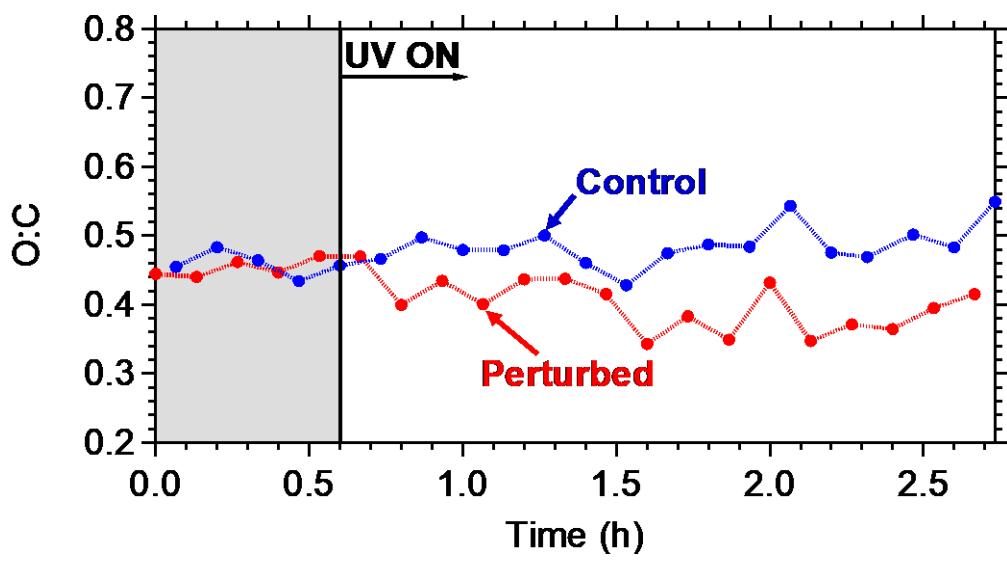


Figure 10. The O:C ratio evolution for the control and the perturbed chamber. The shaded area indicates that the chambers were in the dark.