The BErkeley Atmospheric CO$_2$ Observation Network: Field Calibration and Evaluation of Low-cost Air Quality Sensors

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Abstract. The newest generation of air quality sensors is small, low cost, and easy to deploy. These sensors are an attractive option for developing dense observation networks in support of regulatory activities and scientific research. They are also of interest for use by individuals to characterize their home environment and for citizen science. However, these sensors are difficult to interpret. Although some have an approximately linear response to the target analyte, that response may vary with time, temperature, and/or humidity, and the cross-sensitivity to non-target analytes can be large enough to be confounding. Standard approaches to calibration that are sufficient to account for these variations require a quantity of equipment and labor that negates the attractiveness of the sensors’ low cost. Here we describe a novel calibration strategy for a set of sensors including CO, NO, NO$_2$, and O$_3$ that makes use of multiple co-located sensors, a priori knowledge about the chemistry of NO, NO$_2$, and O$_3$, as well as an estimate of mean emission factors for CO and the global background of CO. The strategy requires one or more well calibrated anchor points within the network domain, but it does not require direct calibration of any of the individual low-cost sensors. The procedure nonetheless accounts for temperature and drift, in both the sensitivity and zero offset. We demonstrate this calibration on a subset of the sensors comprising BEACO$_2$N, a distributed network of approximately 50 sensor “nodes,” each measuring CO$_2$, CO, NO, NO$_2$, O$_3$ and particle matter at 10 second time resolution at approximately 2km spacing in locations surrounding the San Francisco Bay Area.

1 Introduction

In urban environments, air quality has complex spatial and temporal patterns. Diverse emission sources are present with large variations in emission rate and source type on scales of hundreds of meters. In addition, dispersion of pollutants into the urban environment is affected by the topography of the urban landscape and the associated wind flows, which also vary on length scales of $\sim$100 m (Vardoulakis et al., 2003; Lateb et al., 2016). Conventional approaches to air quality monitoring rely on a limited number of relatively high cost instruments that lack the spatial resolution needed to characterize these variations, opting instead to target spatial averages. This averaging hampers our attempts at source attribution and understanding of mixing, chemistry, and human exposure in cities where emissions vary on spatial scales that are small compared to typical observations or models.
One approach to obtaining higher spatial resolution in observations is passive sampling, which has been implemented as a low-cost method using inexpensive sampling devices that can be later analyzed in bulk. Passive samplers do not require electrical power to function properly and are collected and analyzed one to two weeks after deployment. Such protocols provide high spatial resolution but also have significant drawbacks. Spatial resolution is gained at the expense of temporal resolution, and analysis after collection of the samplers is time consuming, thus passive sampling has typically been used only in short duration experiments (e.g. Krupa & Legge, 2000; Cox, 2003). Furthermore, as a result of boundary layer dynamics, passive sampling in urban areas is likely dominated by the high concentrations found at night and relatively insensitive to daytime variability.

Recent developments in low-cost sensors for trace gases and particulate matter, as well as advances in software and hardware enabling low-cost data communication, have made high-density air quality monitoring networks possible. Devices and networks of devices are emerging that are low cost, report at high time resolution, and are capable of long-term deployment, providing potential for improvement over the two major weaknesses of the passive sampling. Examples include metal oxide sensors used to measure O₃, CO, NO₂, and total VOCs (Williams et al., 2013; Bart et al., 2014; Piedrahita et al., 2014; Molchanov et al., 2015; Sadighi et al., 2017), and electrochemical sensors used to measure CO, NO, NO₂, O₃, and SO₂ (Mead et al., 2013; Sun et al., 2015; Jiao et al., 2016; Hagan et al., 2017; Jerrett et al., 2017; Michael et al., 2017). These different low-cost sensor systems were compared during the 1st EuNetAir Air Quality Joint Intercomparison Exercise in 2014 (Borrego et al., 2016). While these studies found low-cost trace gas sensors to be successful at qualitatively characterizing the variability of air quality in an urban area, challenges related to selectivity and stability remain, hindering more quantitative interpretation of the data.

The current generation of low-cost sensors is not as easily tied to a gravimetric calibration standard as many of the passive samplers. Calibration is known to vary with sensor age, temperature, and in some cases humidity. In addition, many of the sensors have responses to gases other than the target analyte (Mead et al., 2013; Spinelle et al., 2015; Cross et al., 2017; Michael et al., 2017; Mijling et al., 2017; Spinhel et al., 2017; Zimmerman et al., 2017). One approach to addressing this challenge is to combine periodic re-calibration and co-location with regulatory reference instruments in the lab or the field (Williams et al., 2013; Molchanov et al., 2015; Jiao et al., 2016; Mijling et al., 2017). Field calibration is preferred as in-lab performance is often a poor approximation of sensor behavior under ambient conditions (Piedrahita et al., 2014; Masson et al., 2015). However, either method requires considerable time investment by trained personnel, especially as the number of sensors increases. The requirement of time and labor consuming calibration then offsets the low-cost advantage of the sensors.
In this paper, we explore an automated, in situ strategy for the calibration of individual sensors embedded in an air quality sensor network that includes both low-cost sensors and anchor points of higher grade, well calibrated instrumentation. The BErkeley Atmospheric CO$_2$ Observation Network (BEACO$_2$N) is a low-cost, high-density greenhouse gas (CO$_2$) and air quality (CO, NO, NO$_2$, O$_3$, and particulate matter) monitoring network located in San Francisco Bay Area, California (see Fig. 1 and Shusterman et al. 2016). As of this writing, BEACO$_2$N consists of approximately 50 sensor “nodes,” deployed with approximately 2 km horizontal spacing. Most of the nodes are mounted on the roofs of schools and museums. In previous work, we described an approach to CO$_2$ sensing and calibration (Shusterman et al. 2016). Here, we focus on CO, NO, NO$_2$, and O$_3$.

We begin by describing laboratory experiments and in-field comparisons to co-located reference instruments that give an initial characterization of the sensors and provide insight into the effects of temperature, humidity, and cross-sensitivity to non-target analytes. Then we describe an in situ calibration procedure that accounts for these variables without requiring co-location with a reference instrument. The calibration procedure is finally verified against regulatory quality measurements not used in the procedure itself.

2 Instrument Description

Details of the node design and deployment are described in Shusterman et al. (2016). Briefly, each BEACO$_2$N node contains a Vaisala CarboCap GMP343 non-dispersive infrared sensor for CO$_2$, a Shinyei PPD42NS nephelometric particulate matter sensor, and a suite of Alphasense electrochemical sensors: CO-B4, NO-B4, either NO$_2$-B42F or NO$_2$-B43F, and either O$_3$-B421 or O$_3$-B431. All sensors are assembled into compact, weatherproof enclosures as shown in Fig. 2. Two 30 mm fans are located on either side of the enclosure to facilitate airflow through the node. A Raspberry Pi microprocessor collects data via a serial-to-USB converter for CO$_2$ and an Adafruit Metro Mini microcontroller for all other sensors. Then, data collected every 5 or 10 seconds is transmitted to a central server using a direct on-site Ethernet connection, a local Wi-Fi network, or an Adafruit FONA MiniGSM cellular module.

The Alphasense B4 electrochemical gas sensing series that we use employs a four-electrode approach. The electrodes are embedded in an electrolyte solution separated from the atmosphere by a semi-permeable membrane. The gas of interest diffuses through the membrane into the electrolyte where it contacts a “working” electrode, and is either oxidized (in the case of NO and CO) or reduced (NO$_2$ and O$_3$). The potential at the working electrode is maintained at a constant value with respect to a “reference” electrode. Electric charge produced at the working electrode is balanced by the complementary redox reaction at a “counter” electrode, generating an electric current. The sensor also contains an “auxiliary” electrode, which shares the working electrode’s catalyst structure, but is isolated from the ambient environment, accounting for...
fluctuations in the background current associated with other processes at the electrode and electrolyte. Subtracting the auxiliary current from the working current gives a corrected current dependent on the gas concentration.

The current detected by the sensors is converted to a voltage that is related to gas concentration using amplifiers in the Individual Sensor Boards (ISBs) provided by Alphasense. Over the mixing ratio range of interest, the sensors’ responses to the gases of interest are approximately linear. We derive mixing ratio from the observed voltages by subtracting an offset and then scaling by a constant (Eqn. 1-4):

$$\text{CO}_{\text{ambient}} = \frac{(V_{\text{CO}} - \text{zero}_{\text{CO}})}{k_{\text{CO}}}$$

$$\text{NO}_{\text{ambient}} = \frac{(V_{\text{NO}} - \text{zero}_{\text{NO}})}{k_{\text{NO}}}$$

$$\text{NO}_2_{\text{ambient}} = \frac{(V_{\text{NO}_2} - \text{zero}_{\text{NO}_2})}{k_{\text{NO}_2}} - r_{\text{NO}_2-\text{NO}_2} \times \text{NO}_2_{\text{ambient}}$$

$$\text{O}_3_{\text{ambient}} = \frac{(V_{\text{O}_3} - \text{zero}_{\text{O}_3})}{k_{\text{O}_3}} - r_{\text{NO}_2-\text{O}_3} \times \text{NO}_2_{\text{ambient}}$$

Here, CO, NO, NO\textsubscript{2}, and O\textsubscript{3} with the subscript “ambient” refer to the gas mixing ratios (ppb) in air; $V_{\text{CO}}, V_{\text{NO}}, V_{\text{NO}_2}$ and $V_{\text{O}_3}$ are the signals (mV) measured by each sensor; zero$_{\text{CO}},$ zero$_{\text{NO}},$ zero$_{\text{NO}_2}$ and zero$_{\text{O}_3}$ indicate the voltage measured in the absence of analyte; and $k_{\text{CO}}, k_{\text{NO}}, k_{\text{NO}_2}$ and $k_{\text{O}_3}$ represent the linear sensitivity factor that converts mV to ppb. Additional terms corresponding to the cross-sensitivities of the NO\textsubscript{2} and O\textsubscript{3} sensors appear in Eqn. 3 and 4, where $r_{\text{NO}_2-\text{NO}_2}$ is the cross-sensitivity of the NO\textsubscript{2} sensor to NO gas and $r_{\text{NO}_2-\text{O}_3}$ is the cross-sensitivity of the O\textsubscript{3} sensor to NO\textsubscript{2} gas.

There are a total of 8 sensitivities and zero offsets, as well as 2 cross-sensitivity terms. All of these may also vary with time, temperature, and humidity. Thus we need a calibration strategy that constrains 10 parameters in a single instant as well as the variation of those 10 parameters in response to the environmental variables. We begin by characterizing the sensors in both laboratory and outdoor environments.

We evaluate BEACO$_2$N in terms of four factors: drift, noise, cross-sensitivity, and temperature dependence. The humidity dependence is included in the temperature dependence, as there is no evidence for independent humidity dependence and relative humidity exhibits an anti-correlation with temperature in the field. This paper examines the behavior of CO-B4, NO-B4, NO$_2$-B42F, and O$_3$-B421. The more recently released NO$_2$-B43F and O$_3$-B431 sensors respond differently; their performance will be assessed in a future study. In the laboratory, a range of mixing ratios of target gases were delivered to a chamber containing the full suite of four Alphasense B4 sensors: CO, NO, NO$_2$, and O$_3$. Zero air was supplied by a Sabio 1001 Compressed Zero Air Source and blended with calibration gases using a ThermoScientific 146i Multi-Gas Calibrator.
Noise – Alphasense reports 2σ noise of ±4 ppb, ±15 ppb, ±12 ppb, and ±15 ppb for CO, NO, NO\textsubscript{2}, and O\textsubscript{3}, respectively over concentrations from 0 ppb to 200 ppb. In our laboratory, noise (±2σ) was measured for ambient ppb levels and was seen to be ±8 ppb for CO, ±4 ppb for NO, ±5 ppb for NO\textsubscript{2}, and ±11 ppb for O\textsubscript{3}.

Cross-Sensitivity – We measured the cross-sensitivity of all 4 of the trace gas sensors to the non-target gases. The NO\textsubscript{2} sensors (NO\textsubscript{2}-B42F) and O\textsubscript{3} sensors (Ox-B421) were the only ones to exhibit sensitivity to other species. The O\textsubscript{3} sensor demonstrated 100% sensitivity to NO\textsubscript{2}. This sensor is now being marketed by Alphasense as an odd oxygen (\(O_\text{x} \equiv O_3 + NO_2\)) sensor. In addition, the NO\textsubscript{2} sensor was found to possess a significant NO sensitivity (130%) that exceeds the cross-sensitivity specified in the Alphasense documentation (<50%). These cross-sensitivities are represented in Eqn. 3 and Eqn. 4.

Temperature Dependence – Electrochemical sensors are known to have temperature dependent sensitivities and zero offsets. Alphasense reports sensitivities and zero offsets for a temperature range between -30 °C and 50 °C. The sensitivities in their data sheets vary with temperature by +0.1 to +0.3 %/K and the zero offsets are indicated to vary little except at high temperatures. We observed similar, but slightly larger variations via in situ comparison to co-located reference instruments. We observed temperature dependence in the sensitivities of +0.3 to +5 %/K and no variation in the zero offset of the CO, NO\textsubscript{2}, and O\textsubscript{3} sensors from 10 °C to 24 °C (Fig. 3). However, the zero offset of the NO sensor exhibited a strong temperature dependence of 0.34 mV/K.

Drift – Two laboratory calibrations were performed roughly 10 weeks apart and the zero offsets and sensitivities are shown in Table 1. Over the 10-week interval, zero drift was equivalent to -15.9 ppb, -2.3 ppb, +15.8 ppb, and -12.7 ppb for CO, NO, NO\textsubscript{2}, and O\textsubscript{3}, respectively. Alphasense reports the stability over time for the zero offset to be < ±100, 0 to 50, 0 to 20, and 0 to 20 ppb yr\textsuperscript{-1} for these sensors, respectively; over this 10 week interval, the observed zero drift was within the range of these specifications. However, it is a large fraction of the annual drift specification and further experiments would be warranted to test whether the zero measured is stable over a full year within the specified tolerances. The drift in the sensitivity (in % of \(k_X\)) was -15.9%, -17.7%, -20.6%, and -53.2%. Alphasense reports <10, 0 to -20, -20 to -40, and < -20 to -40% yr\textsuperscript{-1} for CO, NO, NO\textsubscript{2}, and O\textsubscript{3} calibration factors, respectively. We find that drift for the CO and O\textsubscript{3} sensitivities exceeded the manufacturer specifications, but that the NO and NO\textsubscript{2} sensitivity drifts were within the specified tolerances.

3 Model for Field Calibration

Here, we propose a model for field calibration that leverages (1) useful cross-sensitivities, (2) chemical conservation equations, (3) knowledge of the global and/or regional background of pollutants, and (4) assumptions based on well-known characteristics of urban air quality and local emissions. The result is a calibration procedure for the drift and temperature dependencies of the 10 calibration parameters that does not require co-location with a reference instrument or prior...
laboratory experiments for each sensor. The first constraint we apply is the O3 sensors’ cross-sensitivity to NO2. Laboratory measurements indicate that this cross-sensitivity is 100% and we fix it at that value.

3.1 Regional ozone uniformity to calibrate the NO, NO2 and O3 sensors’ sensitivities

The NO, NO2, and O3 sensitivity can be derived from observations with higher quality instruments at nearby locations. Ozone is a secondary pollutant with small local scale variation, except in the very near field of NO emissions. The Bay Area Air Quality Management District (BAAQMD) maintains four TECO 49i ozone analyzers within the BEACO2N study area (see Fig. 1). We choose the closest site among these four regulatory monitoring sites to provide $O_3$ as a constraint for multiple linear regression of Eqn. 5 (derived from Eqn. 2-4).

$$O_{3_{\text{ambient}}} = \frac{v_{O_3}}{k_{O_3}} - \frac{v_{NO_2}}{k_{NO_2}} + r_{NO-NO_2} \frac{v_{NO}}{k_{NO}} - \text{offset} \quad (5)$$

Here, offset is a combination of the zero offsets of the NO, NO2, and O3 sensors, all of which can be constrained as detailed in Sect. 3.2 below. The sensitivity of O3 and NO2 sensors ($k_{O_3}$ and $k_{NO_2}$), and relationship between the NO-NO2 cross-sensitivity and the sensitivity of the NO sensor ($r_{NO-NO_2}/k_{NO}$) are obtained by doing multiple linear regression of Eqn. 5.

3.2 Use of chemical conservation equations near emissions to calibrate the NO, NO2 and O3 sensors’ sensitivities and zero offsets

We are able to constrain the sensitivity of NO sensors by taking advantage of proximity to local emission sources and the following chemical conservation equations.

$$NO + O_3 \rightarrow NO_2 + O_2 \quad (R1)$$

$$NO_2 + h \nu \rightarrow NO + O \quad (R2)$$

$$O + O_2 + M \rightarrow O_3 + M \quad (R3)$$

These three reactions result in a steady-state relationship among the nitrogen oxides ($NO_x \equiv NO + NO_2$) and ozone. This steady-state operates on a time scale of approximately 100 seconds. On these short time scales, loss of NO (or NO2) and production of NO2 (or NO) is equal and the sum of NO and NO2 is conserved. Similarly, O3, the sum of NO2 and O3 is conserved. Thus we expect that increases (decreases) in NO and O3 are exactly balanced by corresponding decreases (increases) in NO2. Properly calibrated time derivatives of NO vs. time derivatives of NO2 and derivatives of NO2 vs. time derivatives of O3 will have a slope of -1 (see Fig. 4), which can be expressed as Eqn. 6:

$$\frac{\Delta NO_{ambient}}{\Delta NO_2_{ambient}} = \frac{\Delta NO_2_{ambient}}{\Delta O_3_{ambient}} = -\frac{\Delta O_3_{ambient}}{\Delta NO_{ambient}} = -1 \quad (6)$$
We define the Δ quantities as the change in concentration over 10 seconds. This step in the calibration procedure allows the sensitivity for NO to be expressed as a function of the O₃ sensitivity, as ΔNO_{ambient} is equal to ΔV_{NO}/k_{NO}. Since k_{NO₂} is derived in Sect. 3.1, additional constraint for NO₂ sensor can be used as a consistency check.

Next we use these conservation equations to define the zero offsets for the NO and O₃ sensors. At nighttime, reaction R2 does not occur due to the absence of sunlight. In the absence of emissions, the NO concentration goes to zero on nights with sufficient O₃. Conversely, near strong emission sources, NO is found in excess of ozone and the O₃ concentration goes to zero (see Fig. 5). Using this logic, we identify times between 12 am to 3 am when there is zero NO or O₃ and define the zero offsets of the NO and O₃ sensors, using 1-minute averaged data with plumes excluded (see Sect. 3.3 for details of the plume identification procedure).

The NO₂ offset can be determined using the pseudo-steady state (PSS) approximation. We estimate the NO₂ concentration through Eqn. 7:

$$j_{NO₂}[NO₂] = k_{NO→O₂}[NO][O₃]$$

(7)

Here, $j_{NO₂}$ (in units of s⁻¹) is the photolysis rate constant for reaction R2 and $k_{NO→O₂}$ (in units of cm³ molecule⁻¹ s⁻¹) is the rate constant for reaction R1. $[X]$ expresses the concentration of gas $X$ in units of molecules cm⁻³. We use calibrated, 1-minute average NO and O₃ concentrations measured from 12 pm to 3 pm with a time derivative of O₃ near zero to insure that the measurements reflect air that has achieved steady state. The NO₂ concentration at PSS is derived using Eqn. 7 and the NO₂ offset is chosen to insure the calculated and observed NO₂ is equal. NO₂ is also produced through the reaction of HO₂/RO₂ with NO, but this is omitted from the right hand side of Eqn. 7, resulting in a lower bound of NO₂ concentration. Estimated NO₂ is therefore low by about 5% in winter and as much as 30% in summer.

### 3.3 Use of co-emitted gases in plumes to calibrate the CO sensors’ sensitivity

The CO sensor cannot be constrained by cross sensitivity to the other gases. Instead, we constrain the sensitivity by insisting that the median emission factor of CO per unit CO₂ corresponds to median values reported for the U.S. vehicle fleet. We express the CO emission factor ($EF_{CO, ppb ppm⁻¹}$) as in Eqn. 8:

$$EF_{CO} = \frac{ΔCO_{ambient}}{ΔCO₂_{ambient}} = \frac{1}{k_{CO}} \frac{ΔCO}{ΔCO₂_{ambient}}$$

(8)

Our measurements of the concentration of CO₂ are described in Shusterman et al. (2016) and values for $EF_{CO}$ are reported in Dallmann et al. (2013; see Table 2). We constrain the sensitivity of the CO sensors in the network such that the median ΔCO/ΔCO₂ of the plumes with high CO emissions are equal to emission factors characteristic of passenger vehicles.
Figure 6 shows an example of a measured plume and the derived CO emission factor. We identify plumes as the local maximum found in a 10-minute moving window, starting and ending at the local minima. Each plume is a few minutes in duration, representing an emission factor averaged over several vehicles. In the absence of CO measurements, it would be possible to use the ratio of emission factors of NOx to CO, which is also widely measured (McDonald et al., 2013; Civerolo et al., 2016).

3.4 Use of global background to calibrate the CO sensors’ zero offset

To infer the zero offset of the CO sensor, we follow the procedure outlined in Shusterman et al. (2016) for CO sensors. We assume the signal measured at a given site is decomposed as in Eqn. 9:

\[
[CO]_{\text{node}} = [CO]_{\text{background}} + [CO]_{\text{local}} + \text{offset} \tag{9}
\]

The measurement of the pollutant CO \([CO]_{\text{node}}\) is the sum of regional and local signals \([CO]_{\text{background}}\) and \([CO]_{\text{local}}\), respectively, as well as some offset from the true concentration \(\text{offset}\). Assuming the monthly minimum concentration measured at a given site represents \([CO]_{\text{background}}\), this background signal is compared to that measured at a “supersite” of reference instruments located within the network domain, allowing the offset to be derived. We also assume that when \([CO]_{\text{node}}\) as well as \([CO]_{\text{local}}\) is minimum in each day, the concentration measured at a given site has a constant deviation from the background signal. This is a reasonable assumption for the BEACO_2N domain as the dominant wind pattern frequently brings unpolluted air from the Pacific Ocean.

3.5 Temperature dependence and temporal drift

In order to account for the temperature dependence of calibration parameters, we apply the calibration process described in Sect. 3.1 through 3.4 for temperature increments of 1°C to the data in 3-month running window. Then, we are able to define a temperature dependent sensitivity and zero offset, which is used to convert the measured voltages to mixing ratios. In this way, we can also evaluate temporal drift with monthly resolution. The calibration procedure can be repeated for shorter time intervals if wider temperature windows are used.

4 Evaluation with reference observations

We evaluate the efficacy of our calibration method using a BEACO_2N node co-located with reference instruments at the Laney College monitoring site maintained by the Bay Area Air Quality Management District (BAAQMD). Here we consider data collected from February to April 2016, calibrate it according to the procedure described above (following Sect. 3.1 to 3.5), and compare it against the BAAQMD data. Reference data is collected by a TECO 48i CO analyzer and a TECO 42i NOx analyzer. Ozone data from the “Oakland West” location, the closest ozone-monitoring site maintained by BAAQMD, was used for multiple linear regression of Eqn. 5. The zero offset for CO was calculated using BAAQMD data from the
Bodega Bay background site (see Fig. 1; Guha et al., 2016) as local “supersite” data was unavailable during this period. A background site closer to the network would likely improve our ability to constrain the CO zero offset; we installed a reference instrument for that purpose in summer 2017.

In our calibration procedure, the cross-sensitivities and temperature dependence is corrected for better accuracy. Table 3 shows the reduction in mean absolute error (MAE) that results when cross-sensitivity and temperature dependence issues are considered during multiple linear regression of Eqn. 7. Fully calibrated, hourly averaged BEACO2N sensor data is compared to reference data in Fig. 7. For NO, NO2, O3, and CO the mixing ratio measured agrees reasonably well with the reference instrument ($r^2 = 0.88, 0.58, 0.66, and 0.74$ respectively) and is fairly accurate (MAE = 3.25 ppb, 4.00 ppb, 6.88 ppb, and 46.60 ppb respectively. The noise ($\pm 2\sigma$) in the difference between calibrated BEACO2N data and reference data is 10.47 ppb for NO, 10.08 ppb for NO2, 13.81 ppb for O3, and 111.04 ppb for CO. These noise values are dominated by the Alphasense noise except in the case of CO, where noise is evenly split between the low-cost sensors and reference instruments.

5 Examples of network performance

Figure 8 shows a week-long time series of fully calibrated air quality data from four BEACO2N sites in 2017 (see Fig. 1). BEACO2N nodes capture the short-term variability associated with local emissions, superimposed on the diurnal variation caused by mixing and changes in the height of the boundary layer. Large mixing ratios of NO, NO2, and O3 are observed at the Hercules and Ohlone sites, representing strong NOx emissions from an oil refinery nearby. The spatial variability of trace gases observed at these 4 BEACO2N sites provides a richer perspective on emissions when compared to that provided by the one regulatory monitoring site in the vicinity.

The emission ratios of CO and NOx were also investigated using the BEACO2N data from sample locations. Figure 9 shows ratios observed at the Laney College site. The slope of CO/NOx varies from 2.43 to 18.12 across 5 BEACO2N sites, reflecting spatial variations in local sources. Sites near roads with more diesel vehicles, such as Laney College, show lower CO/NOx ratios, as expected given diesel vehicles’ higher NOx emissions. The range of observed CO/NOx emission ratios is similar to the values reported by Mcdonald et al. (2013).

6 Conclusion

Calibration of low-cost sensors is necessary for quantitative analysis. In this paper, we have described a truly low cost, routine in-field calibration method and the subsequent evaluation of a fully calibrated low-cost, high-density air quality sensor network. The Alphasense B4 electrochemical gas sensors are able to detect typical diurnal cycles in gas concentrations as well as short-term changes corresponding to chemical reactions and local emissions. These capabilities of
the sensors are utilized for a field calibration protocol that does not require co-location with reference instrumentation, but does require reference instruments to be sited within the network domain. The calibrated dataset demonstrates the accuracy required to resolve information relevant to urban emission sources, such as CO/NOx emission ratios. Through this work, we can realize the promise of low-cost, high-density sensor networks as a viable approach for atmospheric monitoring.

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References


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Figure 1: Map of San Francisco Bay Area showing current BEACO$_2$N node sites (red), BAAQMD reference sites with O$_3$ measurements (blue), and the BAAQMD Bodega Bay regional greenhouse gas background site (orange). The sites used in this analysis are marked in yellow on the detailed panel.

Figure 2. Current BEACO$_2$N node design.
Figure 3. Representative temperature dependent sensitivities (a) and zero offsets (b) of the Alphasense electrochemical sensors calculated by comparing measurements from BEACO2N node to measurements from reference instrument.

Figure 4. Correlation between (a) the derivative of NO and the derivative of NO$_2$ and (b) the derivative of O$_3$ and the derivative of NO$_2$ at 10 second resolution from a representative week of BEACO2N data; red line has slope of -1.
Figure 5. Representative month of 1-minute averaged NO and O₃ measurements taken between 12 and 3 am; plumes excluded.

Figure 6. Example of CO plume identification and regression against CO₂ to find the CO emission factor. The derived CO emission factor (CO/CO₂) for this example is 15.3 ppb ppm⁻¹.
Figure 7. Time series (top), direct comparison (bottom left), and histogram (bottom right) of hourly averaged (a) NO, (b) NO$_2$, (c) O$_3$, (d) CO mixing ratios from a representative week of BEACO$_2$N and BAAQMD data. Black line in bottom left plot indicates the 1:1 line.
Figure 8. Time series of fully calibrated BEACO$_2$N data from a representative week at 4 Richmond sites deployed in 2017. Observations from the Hercules, Ohlone, Washington, and Madera sites are plotted in red, yellow, blue, and purple, respectively. Particulate matter is converted to units of mass concentration according to Holstuis et al. (2014).
Figure 9. CO vs. NOx measured between 8 am and 10 am.
Table 1. Zero offsets and sensitivities of a representative quartet of Alphasense B4 electrochemical sensors derived via comparison to delivered reference gases during two separate laboratory calibration separated by an approximately 10-week interlude.

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Table 2. Reported emission factors of diesel and gasoline vehicles (Dallmann et al., 2011; Dallmann et al., 2012; Dallmann et al., 2013). Emissions from heavy-duty diesel trucks, which account for <1% of all vehicles, were removed to give the value for “adjusted” light-duty gasoline vehicles.

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<tr>
<th>Vehicle Type</th>
<th>CO emission factor (g kg⁻¹_fuel)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Heavy-duty Diesel Truck</td>
<td>8.0 ± 1.2</td>
</tr>
<tr>
<td>Light-duty Gasoline Vehicles</td>
<td>14.2 ± 0.12</td>
</tr>
<tr>
<td>Adjusted Light-duty Gasoline Vehicles</td>
<td>14.3 ± 0.7</td>
</tr>
</tbody>
</table>

Table 3. Mean absolute error of comparison between regional O₃ and BEACO₂N O₃ measurements derived from multiple linear regression models of increasing complexity.

<table>
<thead>
<tr>
<th>Regression Models</th>
<th>Mean absolute error (ppb)</th>
</tr>
</thead>
<tbody>
<tr>
<td>O₃_True = Vₒ₂/kₒ₂ - offset</td>
<td>Linearity of observed voltages and gas concentration</td>
</tr>
<tr>
<td>O₃_True = Vₒ₂/kₒ₂ - Vₕₒ₂/kₕₒ₂ - offset</td>
<td>O₃ sensor’s cross-sensitivity correction</td>
</tr>
<tr>
<td>O₃_True = Vₒ₂/kₒ₂ - Vₕₒ₂/kₕₒ₂ + rₕₒ₂⁻⁻⁻ Vₕₒ₂/kₕₒ₂ - offset</td>
<td>NO₂ and O₃ sensor’s cross-sensitivity correction</td>
</tr>
<tr>
<td>O₃_True = Vₒ₂/kₒ₂ - Vₕₒ₂/kₕₒ₂ + rₕₒ₂⁻⁻⁻ Vₕₒ₂/kₕₒ₂ - offset</td>
<td>Adding temperature correction</td>
</tr>
</tbody>
</table>