



Sampling of ambient
ice nucleating
particles

L. P. Schenk et al.

This discussion paper is/has been under review for the journal Atmospheric Measurement Techniques (AMT). Please refer to the corresponding final paper in AMT if available.

Characterization and first results of an ice nucleating particle measurement system based on counterflow virtual impactor technique

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Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Received: 11 September 2014 – Accepted: 26 September 2014 – Published: 21 October 2014

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Published by Copernicus Publications on behalf of the European Geosciences Union.

AMTD

7, 10585–10617, 2014

**Sampling of ambient
ice nucleating
particles**

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Abstract

A specific instrument combination was developed to achieve a better microphysical and chemical characterization of atmospheric aerosol particles that have the potential to act as ice nucleating particles (INP). For this purpose a pumped counterflow virtual impactor system called IN-PCVI was set up and characterized to separate ice particles that had been activated on INP in the Fast Ice Nucleus Chamber (FINCH) from interstitial, non-activated particles. This coupled setup consisting of FINCH (ice particle activation and counting), IN-PCVI (INP separation and preparation), and further aerosol instrumentation (INP characterization) had been developed for the application in field experiments. The separated INP were characterized on-line with regard to their total number concentration, number size distribution and chemical composition, especially with the Aircraft-based Laser Ablation Aerosol Mass Spectrometer ALABAMA. Moreover, impactor samples for electron microscopy were taken. Due to the coupling the IN-PCVI had to be operated with different flow settings than known from literature, which required a further characterization of its cut-off-behavior. Taking the changed cut-off-behavior into account, the INP number concentration measured by the IN-PCVI system was in good agreement with the one detected by the FINCH optics for water saturation ratios up to 1.01 (ice saturation ratios between 1.21–1.34 and temperatures between -18 and -26 °C). First field results of INP properties are presented which were gained during the INUIT-JFJ/CLACE 2013 campaign at the high altitude research station Jungfrauoch in the Bernese Alps, Switzerland (3580 m a.s.l.).

1 Introduction

Ice crystals in clouds influence precipitation and the microphysical and thus the radiative properties of clouds. They play an important role for the cloud lifetime, the interactions of clouds with solar radiation, cloud electricity and cloud dynamics. Mixed-phase clouds consisting of supercooled droplets and ice particles exist at altitudes

AMTD

7, 10585–10617, 2014

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



where temperatures warmer than -38°C occur. In such clouds, ice can only be formed heterogeneously, due to the presence of so-called ice nucleating particles (INP) (Vali et al., 2014; DeMott et al., 2011; Pruppacher and Klett, 1997). Known pathways of heterogeneous ice formation are deposition nucleation and condensation, immersion and contact freezing. Field data and modeling studies indicate for many situations that liquid water droplets are a prerequisite for ice formation (Murray et al., 2012; Westbrook and Illingworth, 2011; de Boer et al., 2011; Ansmann et al., 2009). This suggests an important role of immersion and contact freezing processes in atmospheric ice formation. But also sub-saturated nucleation processes (Sassen and Khvorostyanov, 2008) (e.g. deposition nucleation) were found to be an active freezing mechanism under atmospheric conditions. However, the relative importance of the different pathways is not well known at present.

Many species have been identified to act as INP, e.g. mineral dust (e.g., illite, montmorillonite, kaolinite, feldspar), primary biological particles (PBAP), soot, and glassy organics. In laboratory experiments many of these models substances were investigated and their ice forming efficiencies (nucleation temperatures and rates) have been quantified and parameterized (e.g. Murray et al., 2010; Hoose and Moehler, 2012; Atkinson et al., 2013; Wex et al., 2014). However, the type of ambient aerosol particles acting as INP, the importance of their size and the influence of anthropogenically emitted aerosol particles are not well understood. There is still a lack of field measurements concerning the in-situ physio-chemical characterization of atmospheric INP.

In 2011 the Ice Nuclei Research Unit (INUIT) was established with the objective to achieve a more detailed understanding of heterogeneous ice forming processes. The central objective of INUIT is to obtain a better knowledge of ambient aerosol particles serving as INP. Therefore, an ice nucleus counter was connected by means of the counterflow virtual impactor (CVI) technique to online mass spectrometry, and other aerosol measurement techniques, similar to the coupling that had been originally presented by Cziczo et al. (2003) and some years later by Corbin et al. (2012). Corbin et al. (2012) presented measurements from a field study in downtown Toronto (SPORT

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



2011), where they sampled 196 particles that nucleated ice in a continuous flow diffusion chamber (CFDC) by a pumped CVI (PCVI), and analyzed them with the single particle mass spectrometer ATOFMS. Besides dust, also biomass burning and elemental carbon were identified in these particles. However, statistical limitations hampered the data interpretation. In a similar experimental approach a PCVI was combined

with a condensation nucleus counter (CCNC) to investigate cloud droplet residues (Hiranuma et al., 2011; Slowik et al., 2011). The main components of the present study are the INP counter FINCH (Fast Ice Nucleus Chamber; Bundke et al., 2008, 2010), the IN-PCVI (a pumped CVI (BMI, Model 8100, 2011) operated at new flow settings), and the single particle mass spectrometer ALABAMA (Aircraft-based Laser Ablation Aerosol Mass Spectrometer; Brands et al., 2011). This combination of INP activation, ice particle selection, and INP characterization was first established and technically improved under laboratory conditions. Afterwards the combination was deployed for atmospheric measurements at the Jungfraujoch (JFJ) research station to sample and characterize ambient ice nucleating particles at cloud level.

2 Experimental setup – methods

A schematic of the measurement setup which was realized and operated within INUIT (research project RP 2) is shown in Fig. 1. The IN-PCVI (Sect. 2.1) plays the central role as the ice selecting interface between FINCH (Sect. 2.2) and the aerosol instrumentation consisting of ALABAMA (Sect. 2.3), an impactor for offline scanning electron microscopy (SEM, 2.5), a Condensation Particle Counter (CPC, Sect. 2.4) and an Aerosol Particle Sizer (APS, Sect. 2.4). The CPC, APS, and the IN-PCVI constitute the IN-PCVI system.

2.1 Pumped counterflow virtual impactor – PCVI

The CVI used in this study is a pumped CVI (PCVI) from Brechtel Manufacturing Incorporated (Model 8100, 2011). A first characterization was described in Boulter et al. (2006) and another one was presented by Kulkarni et al. (2011). The CVI technique is used to separate large particles from smaller ones and from the gas that originally surrounded the large particles. This is realized by a counterflow that is directed against the IN-PCVI input flow inside the IN-PCVI. Due to their larger inertia larger particles overcome the counterflow and are thus sampled by the IN-PCVI. In the present setup (Fig. 1) large ice crystals are separated from smaller supercooled droplets and interstitial particles. The IN-PCVI input flow corresponds to the FINCH output flow (illustrated in Fig. 1). The flow rates of the IN-PCVI input flow (F_{IF}), counterflow (F_{CF}) and sample flow (F_{SF}) determine the aerodynamic cut-off diameter ($D_{p50\%}$) of the IN-PCVI. This cut-off diameter represents the particle diameter at which particles are sampled with 50 % efficiency. Particles smaller than the $D_{p50\%}$ are sampled with less than 50 % efficiency. Larger ones are collected with higher efficiency. F_{IF} and F_{CF} are adjusted by the pumped flow (F_{PF}) and the add flow (F_{AF}) (Eqs. 1 and 2). The ice particles that penetrate the counterflow are then transferred into the IN-PCVI sample flow where the water is evaporated in particle-free and dry carrier air.

$$F_{CF} = F_{AF} - F_{SF} \quad (1)$$

$$F_{IF} = F_{PF} - F_{CF} \quad (2)$$

Due to the position of the IN-PCVI between FINCH and the aerosol analysis instrumentation (Fig. 1), the IN-PCVI needs to be operated with different flow settings than the ones used previously (Boulter et al., 2006; Kulkarni et al., 2011). Here the PCVI is operated with a sample flow slightly larger than 1 L min^{-1} and with an input flow in the range of 5 L min^{-1} requiring the determination of the cut-off-characteristics for these specific flow rates. For this purpose a calibration of the $D_{p50\%}$ was done with the setup shown in Fig. 2. Polydisperse polystyrene divinylbenzene (DVB) particles (density = 1.05 g cm^{-3} ,

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



formula: $(C_{10}H_{10} \cdot C_8H_8)_x$, Duke Scientific Corporation, now Thermo Scientific) with diameters in a range of 2 to 120 μm (aerodynamic size: Fig. 3) were used as well-defined reference aerosol particles. The polystyrene DVB particles were dispersed manually by a powder dispenser (pushing the balloon which is shown in Fig. 2) and pumped into the IN-PCVI at a prescribed input flow rate of 4, 4.5, or 5 L min^{-1} . For several combinations of input flow rate, counterflow rate (0, 2, 2.5, 3, 3.5 L min^{-1}) and sample flow rate (1, 1.3, 2, and 3 L min^{-1}), at which the IN-PCVI was operated (Table 1), the number size distribution of the test aerosol was measured with an APS. The number size distribution measured with the counterflow being switched off was taken as reference. It was normalized to a maximum of 1 and all cut-off size distributions (i.e., F_{CF} switched on) measured for the same inlet and sample flow were scaled to match the right branch of the reference size distribution. This approach was chosen to minimize the error due to size-dependent particle losses in the inlet region of the IN-PCVI. The calibration runs were repeated several times for averaging the aerodynamic size distribution and thus to minimize the error due to the manual dispersion of the calibration aerosol.

The calibration curves of the most common sample and input flow settings of the INUIT-JFJ/CLACE 2013 campaign (Run 4–7, Table 1) are illustrated in Figs. 3 and 4. Figure 3 shows the normalized APS measured aerodynamic size distribution, here for a fixed F_{IF} and F_{SF} , while F_{CF} is varied. As expected, for larger counterflows the cut-off is shifted to larger sizes. The transmission efficiency (TE, sampling efficiency of particles of a certain size passing the IN-PCVI) is defined by the ratio of the normalized sample flow concentration N_{out} with counterflow switched on and the normalized reference concentration N_{in} ($F_{CF} = 0$) (Eq. 3).

$$TE = \frac{N_{out}(d_p)_{norm.}}{N_{in}(d_p)_{norm.}} \quad (3)$$

Figure 4 shows the transmission efficiency curves for the measurements shown in Fig. 3. The vertical dashed lines mark the resulting cut-off-diameter, $D_{p50\%}$. It can be seen that with increasing F_{CF} from 0.5 to 3.5 L min^{-1} the $D_{p50\%}$ increases from 5 to

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



6.5 μm . The behavior of the $D_{p50\%}$ was also studied for different input and sample flows. The resulting $D_{p50\%}$ for all flow variations were in a range between 5.2 and 8.4 μm (Fig. 5). It is evident that a change of the $D_{p50\%}$ is most sensitiv to a change of F_{IF} compared to a change of F_{SF} or F_{CF} (slopes of regressions for the chosen flow regime are shown in Fig. 5a–c). In Fig. 5a, $D_{p50\%}$ results determined by Kulkarni et al. (2011) are displayed for comparison. Since F_{IF} in our experiments is lower ($F_{\text{IF}} = 5 \text{ L min}^{-1} < F_{\text{IF(Kulkarni)}} = 6.7 \text{ L min}^{-1}$), the absolute $D_{p50\%}$ values are higher. Nevertheless, the same relative change in $D_{p50\%}$ (same slope) is found for the two F_{IF} settings.

The cut-off diameters for the new flow parameters (Table 1) represent an extended characterization of the commercial PCVI from Brechtel Inc., clearly showing that this device is working properly in the flow regime required for the operation of the IN-PCVI during the INUIT-JFJ/CLACE 2013 field campaign.

2.2 Fast Ice Nucleus Chamber (FINCH)

FINCH was developed and built at the Goethe University of Frankfurt. It is an in situ counter for ice nucleating particles, which is operated by mixing air flows with different humidity and temperature to achieve supersaturation (with respect to water (S_{wat_F}) and with respect to ice (S_{ice_F})) (Bundke et al., 2008). The main component of the device is a temperature-controlled, stainless steel growth chamber with a length of 0.8 m that can be cooled down to -65°C . Sampled aerosol particles are activated and grow to macroscopic ice particles or supercooled droplets depending on the temperature (T_F) and supersaturation (S_{ice_F}) inside the chamber.

Depending on the mixed air flow rate the aerosol particles typically need ~ 10 s to pass the chamber. The (grown) particles are counted in an optical particle counter mounted directly below the chamber (BIO-IN-OPC; Bundke et al., 2010). Based on scattering properties a distinction between water droplets and ice particles is possible (P44/P11 ratio of the scattering matrix; Hu et al., 2003). The current setup of the

detector consists of a 405 nm laser, which stimulates the particles to fluoresce as well. In this study the outlet of the BIO-IN-OPC was directly connected to the IN-PCVI.

After several hours of operation the measurements with FINCH are interrupted for a short heating period to melt the ice that had built up in the inlet and thus resulted in a reduced or plugged flow. After every heating period the saturation ratio inside FINCH is automatically re-established to the set value, which can take up to an hour. During operation S_{iceF} is adjusted continuously as a consequence of changing ambient temperature and relative humidity.

2.3 Aircraft-based laser ablation aerosol mass spectrometer (ALABAMA)

ALABAMA is a single particle laser ablation instrument to detect the chemical composition, mixing state and size of aerosol particles in a range from 150–900 nm (Brands et al., 2011). It was built and characterized at the Max Planck Institute for Chemistry (MPIC) Mainz. The particles are detected and sized by two continuous lasers at a wavelength of 405 nm (InGaN Blu-Ray laser). Thereafter, a 266 nm wavelength pulsed Nd-YAG-laser is used to evaporate the aerosol particles and ionize the components. A bipolar, Z-shaped time-of-flight mass spectrometer (Tofwerk) generally detects positive and negative ions. During the INUIT-JFJ/CLACE 2013 campaign only positive ions were detected due to technical issues. It is used to measure the chemical composition of FINCH-detected INP, which are separated, sampled and released by the IN-PCVI.

2.4 Microphysical aerosol instrumentation

For a microphysical characterization of the INP a condensation particle counter (CPC TSI 3010) and an aerodynamic particle sizer (APS TSI 3321) were connected downstream the IN-PCVI. The CPC measures the number concentration of particles that are larger than 0.01 μm in diameter.

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



to the following one. As a main result of these tests, the FINCH closed loop had to be switched off and the FINCH aerosol flow had to be directly controlled by the IN-PCVI pump flow. This led to stable pressure conditions inside the coupled FINCH + IN-PCVI flow system. Additionally, it was found that changes in the IN-PCVI – FINCH flows caused fluctuations in the supersaturation of FINCH, which sometimes resulted in a frozen inlet and thus blocking of the growth chamber. Therefore, the FINCH – IN-PCVI flows were kept constant during single measurement runs.

2.7 Atmospheric measurements at the high Alpine research station Jungfraujoch

The combination of INP activation and detection (FINCH), separation/preparation (IN-PCVI), and characterization (aerosol instrumentation) was deployed in January/February 2013 during the INUIT-JFJ/CLACE-2013 joint measurement field campaign (Schneider et al., 2014) at the Sphinx Laboratory of the high Alpine research station Jungfraujoch (JFJ, Bernese Alps, Switzerland, 3580 m a.s.l.). The combination of FINCH, IN-PCVI, and aerosol instruments was deployed at this site to sample aerosol particles inside mixed-phase or, sometimes, even entirely glaciated clouds, where supercooled drops and small ice particles were evaporated during collection by heated total aerosol inlet (operated by Paul Scherrer Institute, Villigen; Weingartner et al., 1999). Also ambient background aerosol particles, which are present during cloud free time periods, are sampled at these altitude that are realistic for the mixed-phase cloud formation at mid latitudes.

measured by the IN-PCVI CPC ($N_{\text{INP}_{\text{IN-PCVI}}}$, same 10 min averages). The data points are subdivided into 3 classes with regard to the prevailing FINCH water saturation ratio:

$S_{\text{wat}_F} < 1.0$ (squares), $1.0 < S_{\text{wat}_F} < 1.1$ (circles) and $1.1 < S_{\text{wat}_F} < 1.2$ (crosses).

5 The 1 : 1 line indicated in Fig. 7 shows that there exists a very close correlation between $N_{\text{INP}_{\text{FINCH}}}$ and $N_{\text{INP}_{\text{IN-PCVI}}}$ for $S_{\text{wat}_F} < 1.0$ (squares), which implies that the residue of each ice particle grown in FINCH is transferred with high efficiency through the IN-PCVI and all other particles exiting FINCH (supercooled droplets, unactivated particles) are diverted into the F_{PF} of the IN-PCVI. With increasing water saturation ratio, however,
10 $N_{\text{INP}_{\text{IN-PCVI}}}$ concentration exceeds $N_{\text{INP}_{\text{FINCH}}}$. Since it is not likely that more ice nucleating particles exist after the IN-PCVI than there were ice particles counted after FINCH, the most probable explanation is that some liquid supercooled droplets that are formed in FINCH reach the same size as the ice particles at higher saturation. Thus, they cannot be pre-segregated by the IN-PCVI and become erroneously counted and sampled
15 as INP. In order to estimate the magnitude of this effect, power regressions (with an exponent equal 1) were calculated for each class and plotted in Fig. 7. These indicate contribution of large droplet residuals 0, 45, and 63% for the intended INP sampling with respect to the three S_{wat_F} classes.

20 Table 2 gives a more detailed verification of the droplet contamination effect. Again power regressions are derived from the $N_{\text{INP}_{\text{FINCH}}}$ to $N_{\text{INP}_{\text{IN-PCVI}}}$ relationship but now separately for a S_{wat_F} increment of 0.01. The desired regression close to 1 is only achieved for $S_{\text{wat}_F} \leq 1.01$, which denotes an ice saturation between 1.21 and 1.3 for the adjusted temperatures. However, the uncertainty of the regression slope includes 1 still for a $S_{\text{wat}_F} \leq 1.06$ ($1.21 < S_{\text{ice}_F} < 1.34$). Accepting a ratio of one drop residual out of
25 three INP_{IN-PCVI} would allow to take into account all measurements up to $S_{\text{wat}_F} \leq 1.08$ ($1.21 < S_{\text{ice}_F} < 1.34$). For all INP results obtained by the coupled system these limitations and uncertainties have to be taken into account.

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



3.2 First measurements of INP properties

Having proven the feasibility and discussed the operational limitations of the FINCH + IN-PCVI coupling, now first exemplary results of INP properties obtained with this experimental setup during the INUIT-JFJ/CLACE-2013 campaign are presented. Identical to the experimental setup described in Sect. 3.1 ambient particles as well as residues of supercooled drops or ice particles in the presence of clouds were sampled by the heated total aerosol inlet, to which the combination of FINCH, IN-PCVI, and aerosol sensors was connected to. During all measurements at the JFJ the IN-PCVI cut-off diameter was adjusted in the characterized range, which is shown in Fig. 5a–c. Figure 8 shows an INP time series from a 4 h case study on 9 February 2013. The data points are again 10 min mean values and meet the above described criterion of the FINCH saturation ratio varying less than 1% in 300 s. Within this period T_F was adjusted in a range from -21 to -23.5°C and S_{ice_F} to ~ 1.1 , respectively. Thus, FINCH was operated at water sub-saturated conditions, i.e. deposition nucleation and/or immersion freezing of highly concentrated solutions are the prevailing heterogeneous nucleation mechanisms inside FINCH. Consistent with the findings in Sect. 3.1, the FINCH and IN-PCVI INP concentrations agree very well in this case study increasing from 5 to 25 L^{-1} . The reason for the increase of the INP concentration by a factor of 5 within 3 h is not clear, but a decisive change in the air mass can be ruled out.

Another measure for the INP number concentration is inferred from integrating the INP number size distribution measured by the APS (Fig. 8). The lower size detection limit of the APS is $0.55\ \mu\text{m}$, i.e., the APS $N_{\text{INP}_{\text{IN-PCVI}}}$ refers to all INP_{IN-PCVI} larger than this diameter. The variation of the concentration of these large INP in time shows the same increasing trend but on a substantially lower level between 0 to 4 L^{-1} , which is a factor of 7 below the values of the total INP concentration. Hence, it can be concluded that only 13% of the sampled INP are larger than $0.55\ \mu\text{m}$ and the majority of the INP (87%) are smaller for the situation encountered in this case study. Tests of the reduced counting efficiency in the lower APS channels (555–700 nm) showed only

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



showed an excellent agreement for water saturation ratios ≤ 1.01 ($1.21 < S_{\text{iceF}} < 1.3$). This implies that ice particles nucleated in FINCH are efficiently separated by the IN-PCVI from the interstitial particles and supercooled droplets that are also present at the FINCH outlet, and that consequently only INP are selected by the IN-PCVI for further analysis. At higher water saturation ratios higher INP concentrations were measured with the IN-PCVI CPC than with the FINCH optics, which may be attributed to supercooled drops growing into the same size range as the ice particles and can therefore not be rejected by the counterflow. This effect is estimated to result in an overestimation of INP concentrations by about 25 % for FINCH water saturation ratios up to 1.08 ($1.21 < S_{\text{iceF}} < 1.34$).

Ambient INP properties were inferred from the measurements carried out during the INUIT-JFJ/CLACE 2013 field campaign. Restricting the considered measurements to water saturation ratios ≤ 1.0 , i.e., considering deposition nucleation and/or immersion freezing of highly concentrated solutions, INP concentrations of up to 40 L^{-1} were measured (S_{iceF} between 1.0 and 1.3, temperatures between -15 and -28 °C) over the campaign duration. In a 4 h case study 87 % of the INP were found to be smaller than $0.55 \mu\text{m}$. From the shape of the frequency distribution of INP diameters it can be concluded that the ice nucleating efficiency increases with particle size.

The combination of FINCH + IN-PCVI + ALABAMA resulted in 7 mass spectra of INP, which cannot be statistically evaluated, but represent a successful proof-of-concept for the system. A clear need to improve the counting efficiency of the FINCH + IN-PCVI + ALABAMA combination has to be stated when deploying the system in environments with low INP concentrations. However, for laboratory applications and use in environments with high INP concentrations, the FINCH + IN-PCVI + ALABAMA combination can already be applied in the current development stage.

Acknowledgements. This project is funded by the German Research Foundation (Research Unit INUIT, FOR 1525, grants STR 453/7-1, BU 1432/4-1, SCHN1138/2-1 and EB 383/3-1 and DFG grant ME 3534/1-2). The authors thank the International Foundation High Altitude Research Station Jungfraujoch and Gornergrat (HFSJG). We thank T. Klimach for help with

the ALABAMA operation during the JFJ campaign. Also, we thank Thomas Conrath for his intensive technical support.

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Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



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Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



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Sampling of ambient ice nucleating particles

L. P. Schenk et al.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)

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- 10

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Table 1. Flow setup of the IN-PCVI (counterflow (F_{CF}), input flow (F_{IF}), sample flow (F_{SF})) resulting in different cut-off-diameters ($D_{p50\%}$).

Run	F_{CF} (L min ⁻¹)	F_{IF} (L min ⁻¹)	F_{SF} (L min ⁻¹)	$D_{p50\%}$ (μm)
1	3	5	1	5.6
2	3	5	2	6.5
3	3	5	3	7.9
4	2	5	1.3	5.2
5	2.5	5	1.3	6
6	3	5	1.3	6.2
7	3.5	5	1.3	6.5
8	3	4	1.3	8.4
9	3	4.5	1.3	7.8
10	3	5	1.3	6.2

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Table 2. Slope a of the $N_{\text{INP}_{\text{IN-PCVI}}} - N_{\text{INP}_{\text{IN-PCVI}}}$ scatter plot regression depending on the considered water saturation range, the standard deviation (SD) of a , the derived relative droplet contaminations (RDC) and corresponding ice saturation ratios for the investigated temperature range.

S_{wat_F} range	a	SD(a)	RDC (%)	$S_{\text{ice}_F}(-18^\circ\text{C}) - S_{\text{ice}_F}(-26^\circ\text{C})$
≤ 1	0.94	0.05	0	1.2–1.3
≤ 1.01	1.03	0.22	3	1.21–1.31
≤ 1.02	1.12	0.26	12	1.22–1.33
≤ 1.03	1.09	0.22	9	1.24–1.34
≤ 1.04	1.08	0.2	8	1.25–1.35
≤ 1.05	1.13	0.2	13	1.26–1.37
≤ 1.06	1.17	0.18	17	1.27–1.38
≤ 1.07	1.18	0.17	18	1.28–1.39
≤ 1.08	1.24	0.14	24	1.3–1.41
≤ 1.09	1.26	0.13	26	1.31–1.42
≤ 1.1	1.32	0.1	32	1.32–1.43
≤ 1.2	1.53	0.07	53	1.44–1.56

[Title Page](#)
[Abstract](#)
[Introduction](#)
[Conclusions](#)
[References](#)
[Tables](#)
[Figures](#)
[Back](#)
[Close](#)
[Full Screen / Esc](#)
[Printer-friendly Version](#)
[Interactive Discussion](#)


Sampling of ambient ice nucleating particles

L. P. Schenk et al.

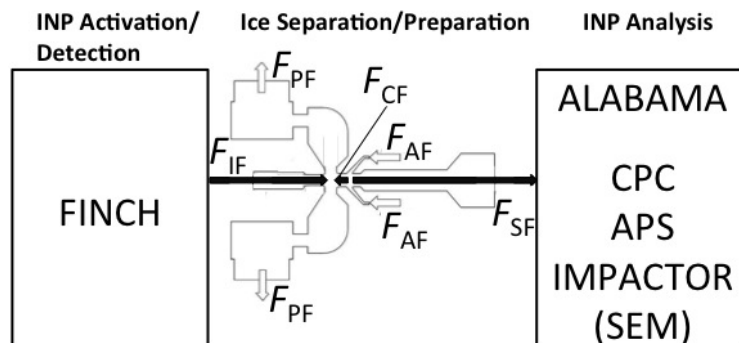


Figure 1. Schematics of the coupled FINCH – IN-PCVI – analysis setup. FINCH activates the INP and counts the grown ice crystals. The IN-PCVI separates these ice particles from non-activated aerosol particles and smaller supercooled droplets, which are also formed inside FINCH. The released INP are transferred to the aerosol sensors for chemical and physical analysis. Flows inside the IN-PCVI are illustrated by arrows and described in the text.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



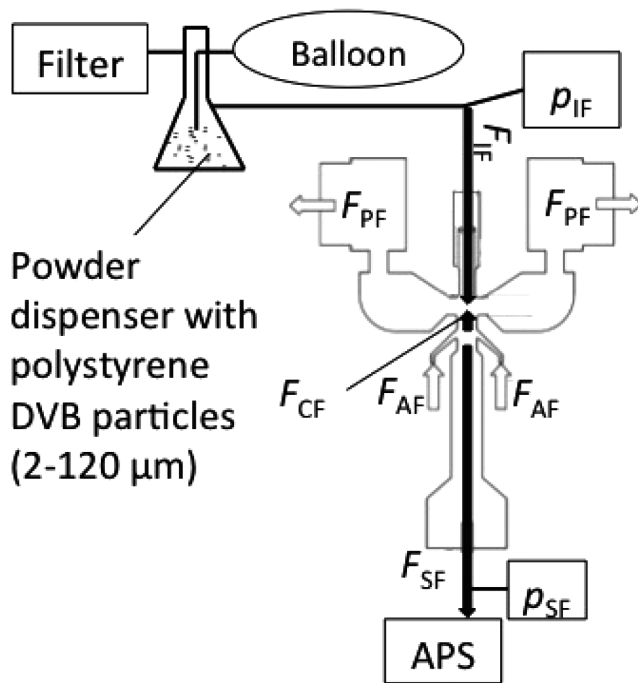


Figure 2. Sketch of the measurement setup for the IN-PCVI $D_{p50\%}$ characterization. A pump bottle is used to disperse polystyrene DVP particles (2–120 μm). The APS of the IN-PCVI system connected downstream of the IN-PCVI measured the reference size distribution (F_{CF} switched off) and the size distribution when the counterflow was switched on. The pressure is measured up- and downstream the IN-PCVI to ensure stable flow conditions (ρ_{IF} and ρ_{SF}).

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



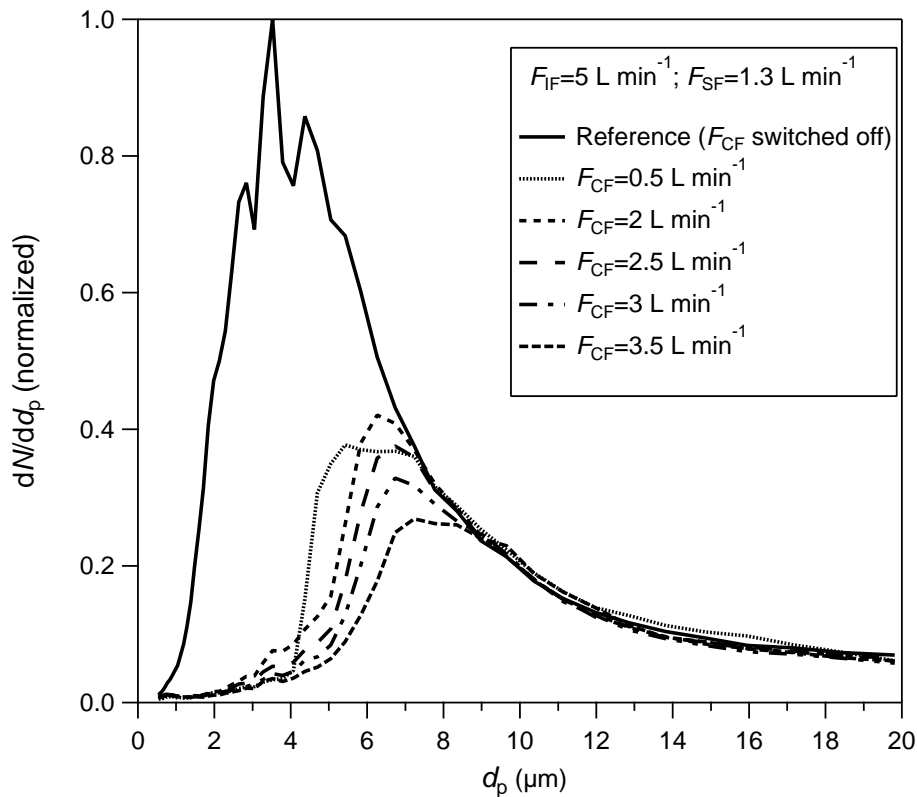


Figure 3. Polystyrene DVB reference number size distribution (solid line) and number size distributions at different counterflows (see legend). All number size distributions were measured by the APS and were normalized to a maximum of 1.

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



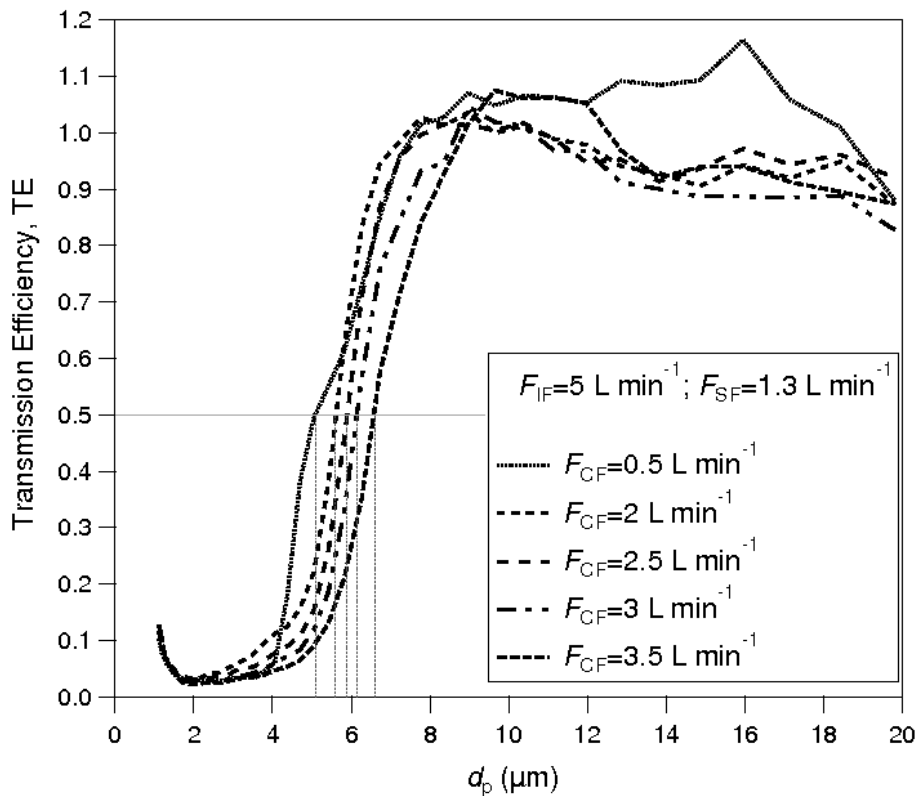


Figure 4. Transmission efficiency of the IN-PCVI derived from the number size distributions shown in Fig. 3. Vertical lines indicate the variation of $D_{p50\%}$ as a function of the counterflow.

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

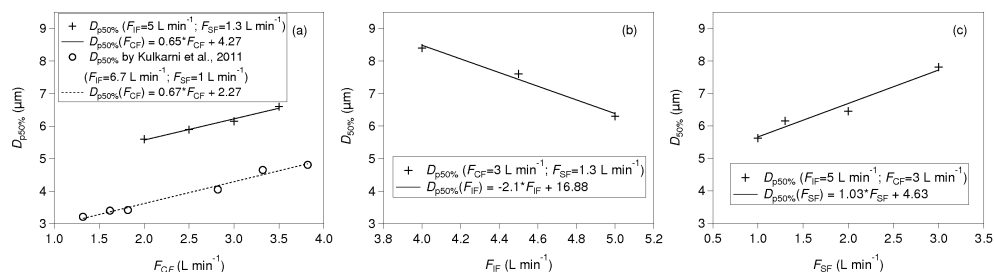


Figure 5. The IN-PCVI cut-off diameter, $D_{p50\%}$ for a changing (a) counterflow F_{CF} , (b) input flow F_{IF} and (c) sample flow F_{SF} . In (a) the variation of the $D_{p50\%}$ with F_{CF} as characterized by Kulkarni et al. (2011) is plotted as circles with a dashed regression line.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



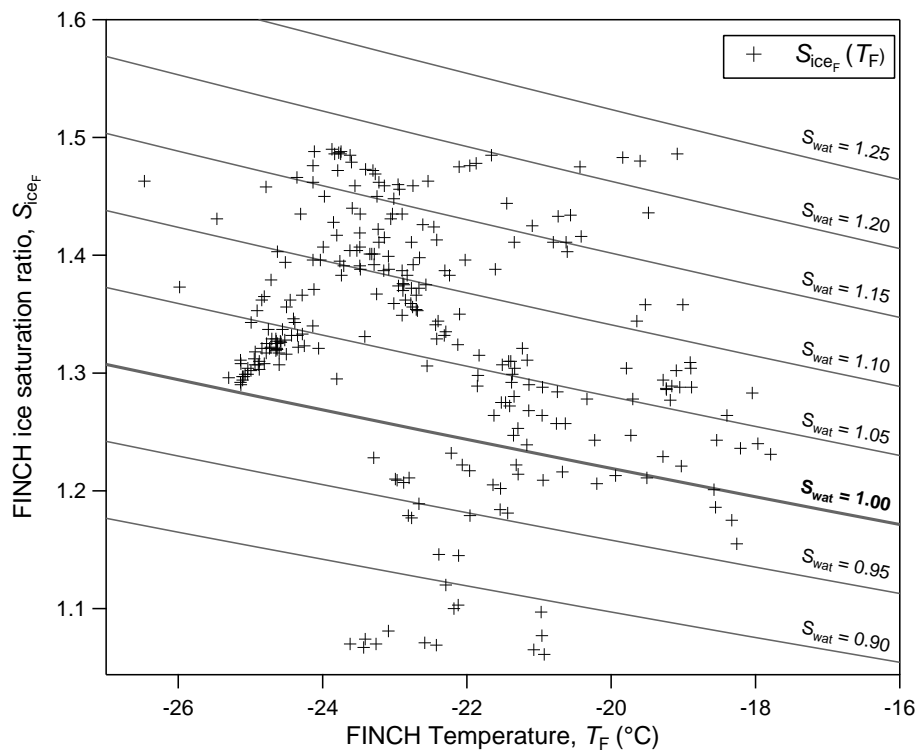


Figure 6. Ice activation conditions in FINCH cover a range of combinations of temperatures (T_F) and ice saturation ratios (S_{iceF}). The majority of measurements was conducted at conditions supersaturated with respect to water (lines of constant S_{wat_F} are plotted in grey (0.05 steps)).

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures

◀

▶

◀

▶

Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



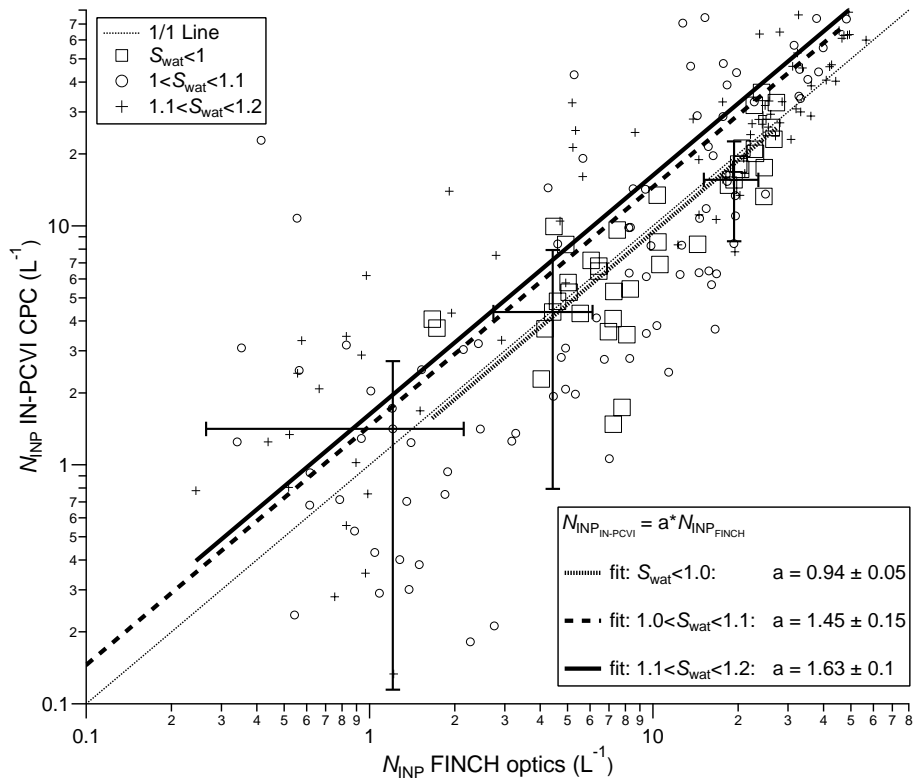


Figure 7. Scatter plot of the INP 10 min averaged number concentrations measured by the FINCH optics and the CPC of the IN-PCVI system, respectively. The concentrations are subdivided into three different water saturation ranges: $S_{wat_F} < 1.0$ (squares), $1.0 < S_{wat_F} < 1.1$ (circles) and $1.1 < S_{wat_F} < 1.2$ (crosses). The power regression curves (exponent equal 1) for these three classes are plotted as lines: $S_{wat_F} < 1.0$ (dotted line), $1.0 < S_{wat_F} < 1.1$ (dashed line) and $1.1 < S_{wat_F} < 1.2$ (solid line). For every number concentration range an example of the standard deviation is indicated by error bars.

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

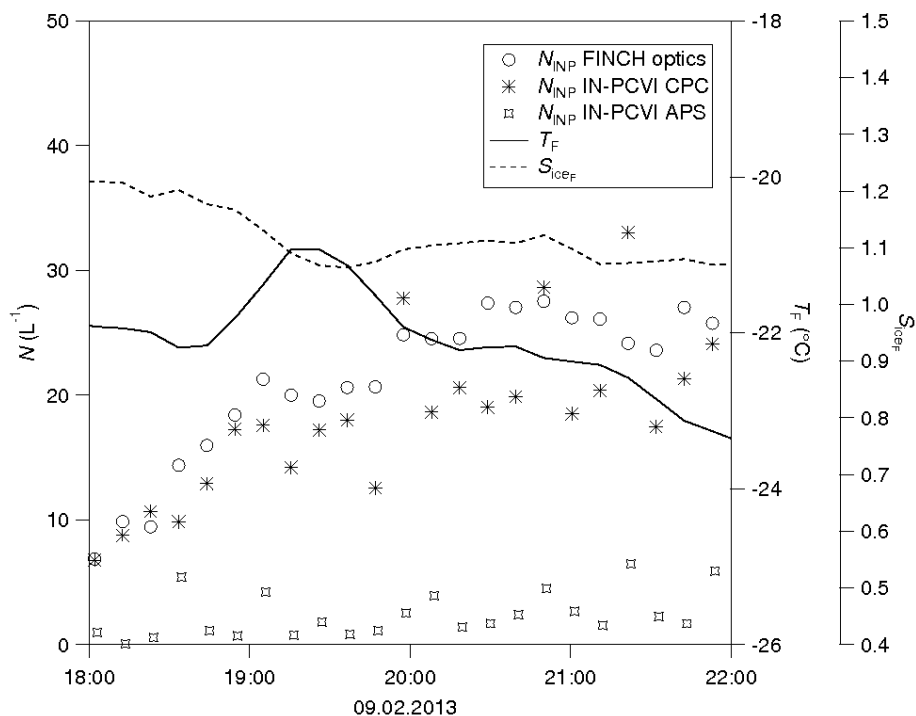


Figure 8. Time series of the INP number concentration (10 min averages) measured by the FINCH optics and by the IN-PCVI system (CPC and APS). The FINCH thermodynamic conditions are plotted as solid (temperature) and dashed (ice saturation) lines on the axes on the right hand side.

Title Page

Abstract

Introduction

Conclusions

References

Tables

Figures



Back

Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion



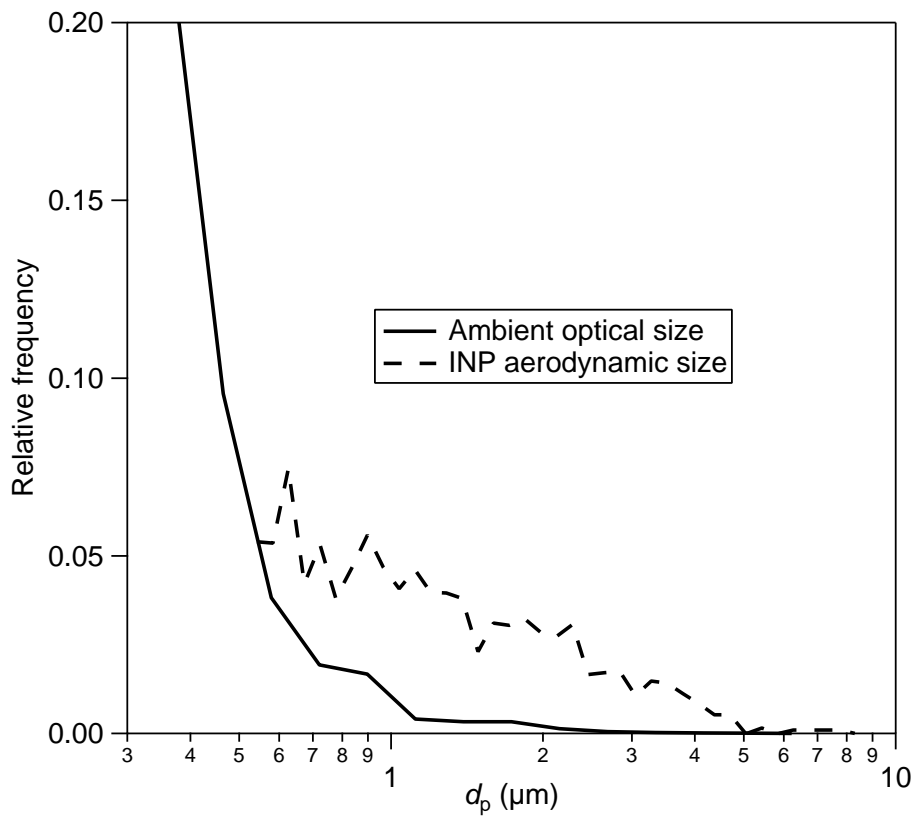


Figure 9. Relative frequency of the FINCH-INP sizes measured with the APS over the whole campaign period (dashed line) in comparison to the relative frequency of ambient aerosol particle sizes measured with an OPS (solid line).

Sampling of ambient ice nucleating particles

L. P. Schenk et al.

Title Page	
Abstract	Introduction
Conclusions	References
Tables	Figures
◀	▶
◀	▶
Back	Close
Full Screen / Esc	
Printer-friendly Version	
Interactive Discussion	



Sampling of ambient ice nucleating particles

L. P. Schenk et al.

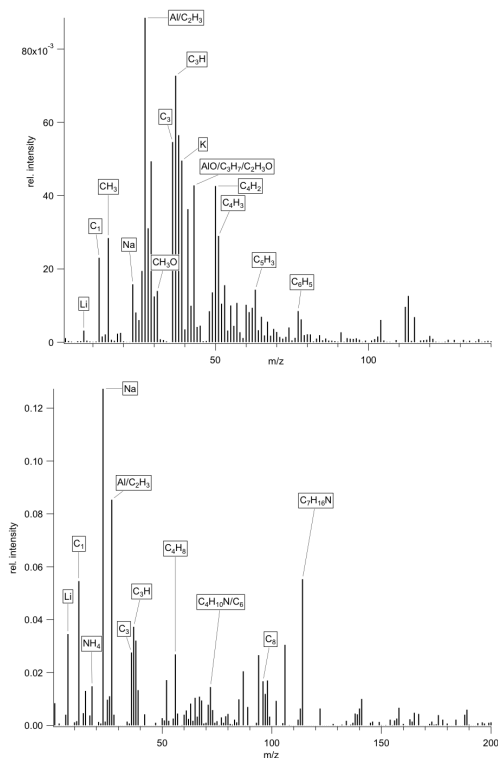


Figure 10. Examples for INP mass spectra measured online with the single particle mass spectrometer ALABAMA behind the FINCH + IN-PCVI. Both particle spectra are dominated by organic ions, but elements like Li and Al might also indicate that these particles may be mineral dust coated with organic matter.

[Title Page](#)[Abstract](#)[Introduction](#)[Conclusions](#)[References](#)[Tables](#)[Figures](#)[◀](#)[▶](#)[◀](#)[▶](#)[Back](#)[Close](#)[Full Screen / Esc](#)[Printer-friendly Version](#)[Interactive Discussion](#)