



**Turbulent fluxes
errors over the
tropical Zongo
glacier**

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A study of turbulent fluxes and their measurement errors for different wind regimes over the tropical Zongo glacier (16° S) during the dry season

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Abstract

Over glaciers in the outer tropics, during the dry winter season, turbulent fluxes are an important sink of melt energy due to high sublimation rates, but measurements in stable surface layers, in remote and complex terrains remain challenging. Eddy-covariance (EC) and bulk-aerodynamic (BA) methods were used to estimate surface turbulent heat fluxes of sensible (H) and latent heat (LE) in the ablation zone of the tropical Zongo glacier, Bolivia (16° S, 5080 m a.s.l.), from 22 July to 1 September 2007. We studied the turbulent fluxes and their associated random and systematic measurement errors under the three most frequent wind regimes. For nightly, density-driven katabatic flows, and for strong downslope flows related to large-scale forcing, H generally heats the surface (i.e., is positive), while LE cools it down (i.e., is negative). On average, both fluxes exhibit similar magnitudes and cancel each other out. Most energy losses through turbulence occur for daytime upslope flows, when H is weak due to small temperature gradients and LE is strongly negative due to very dry air. Mean random errors of the BA method (6% on net $H + LE$ fluxes) originated mainly from large uncertainties in roughness lengths. For EC fluxes, mean random errors were due mainly to poor statistical sampling of large-scale outer-layer eddies (12%). The BA method is highly sensitive to the method used to derive surface temperature from long-wave radiation measurements and underestimates fluxes due to vertical flux divergence at low heights and nonstationarity of turbulent flow. The EC method also probably underestimates the fluxes, but to a lesser extent, due to underestimation of vertical wind speed and to vertical flux divergence. For both methods, when H and LE compensate each other in downslope fluxes, biases tend to cancel each other out or remain small. When the net turbulent fluxes ($H + LE$) are the largest in upslope flows, nonstationarity effects and underestimations of the vertical wind speed do not compensate, and surface temperature errors are important, so that large biases on $H + LE$ are expected when using both the EC and the BA method.

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1 Introduction

Surface turbulent heat fluxes play a significant role in the energy balance of mountain glaciers (Sicart et al., 2008; Anderson et al., 2007; Gillett and Cullen, 2011), a crucial calculation for assessing melt and mass balance using meteorological variables.

5 Commonly, turbulent fluxes are estimated with the bulk-aerodynamic (BA) method, and only a few studies have relied on direct measurements with the eddy-covariance (EC) method (e.g., Cullen et al., 2006; Van den Broeke et al., 2009; Conway and Cullen, 2013; Litt et al., 2014). Over mountain glaciers, several characteristics of turbulent flows challenge the measurement of turbulent fluxes, such as flux divergence between
10 the surface and the instruments under frequent katabatic winds (Grisogono and Oerlemans, 2002), non-equilibrium surface-layers related to large-scale orographic disturbances (Smeets et al., 1999), temperature overestimates due to strong shortwave radiation and large surface albedo (Huwald et al., 2009), or intermittency in weak-wind and strong stable stratification (Mahrt, 2007). These characteristics can cause significant errors in estimates of turbulent fluxes and thus in the energy balance.

On the Alpine Pasterze Glacier, Smeets et al. (1999) found evidence for the influence of outer-layer turbulent structures on the surface layer that impacted turbulent fluxes, and Denby and Greuell (2000) showed that under katabatic winds, the BA method underestimated surface fluxes, but less so than when applying the profile method between
20 two measurements levels in the air. Conway and Cullen (2013) studied the influence of uncertainties in roughness lengths, surface temperature and the choice of stability corrections on the calculation of surface-energy balance on a glacier in the Southern Alps of New Zealand. Sicart et al. (2014a) studied impacts of uncertainties in roughness lengths and the ill-defined zero-reference level on turbulent fluxes on the tropical
25 Zongo glacier in Bolivia. On the same glacier, Litt et al. (2014) compared results of the BA method to those of the EC method and attributed large underestimates of turbulent sensible heat flux (H) by the BA method to the influence of katabatic flow oscillations or

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a wind-speed maximum is frequently observed at low height. Strong synoptic forcing causes strong winds at the glacier surface, while complex outer-layer interactions with the surface-layer occur (Litt et al., 2014). During afternoons of the dry season, upslope valley winds are frequently observed, while the temperature inversion is less marked.

5 Net turbulent surface heat flux ($H + LE$) and associated errors may strongly depend on these wind-regime characteristics. A comprehensive review and quantification of sources of uncertainties, and comparison of these errors with net turbulent fluxes under different wind regimes, is required to improve uncertainty assessment in energy balance studies.

10 This study focuses on some of the most important errors expected in flux estimates by the BA and EC methods over the tropical Zongo glacier. We describe measurements from a micro-meteorological field campaign performed in the ablation area during the 2007 dry season from July to September and associated data analysis. Hourly mean incident and reflected shortwave and longwave radiation and 2 m temperature, wind speed and humidity were measured, as were 2 m EC data and temperature and wind-speed vertical profiles with a 6 m mast. For each of the three wind regimes observed, i.e., pure katabatic flows, strong downslope flows and upslope flows, we derived H and LE using both the BA and EC methods and calculated their main systematic and random measurement errors. We then identified the error sources that most impacted estimates of net turbulent flux and those of secondary importance. Finally, for each wind regime, we discuss changes in its net turbulent fluxes and the influence of errors.

2 Location and data

2.1 Site and measurements

25 The site and field campaign are extensively described in Sicart et al. (2014a) and Litt et al. (2014). A short description is given here for consistency. The Zongo glacier is a small (approximately 1.8 km^2), high-altitude (4800–6000 m a.s.l.) Andean Glacier

degrees above 0°C, which results in a nearly neutral thermal stratification in the first few meters above the surface. During the experiment, wind speed was moderate under these conditions: a mean of 2.1 ms⁻¹, with a maximum of 6.8 ms⁻¹.

For these three wind regimes, low-frequency perturbations affect the surface-layer flow (Litt et al., 2014). The mean cospectra of vertical wind speed, w , with potential temperature, θ , and those of w with specific humidity, q , are plotted in Fig. 2 against normalized frequency $n = fz/\bar{u}$, where f is frequency, u is the horizontal wind speed, z is the measurement height, and the overline indicates a temporal average over a 1 h run. These cospectra reveal that the low-frequency perturbations observed affect the turbulent fluxes since they show stronger contributions at low frequency (below $n = 10^{-1}$) than the reference curve of Kaimal et al. (1972), which was measured under ideal undisturbed conditions. At low wind speeds, in pure katabatic flows, the low-frequency perturbations likely result from oscillations in the katabatic flow (McNider, 1982). When outer-layer forcing is strong, these oscillations probably originate from interactions between outer-layer eddies and the surface layer (Högström et al., 2002; McNaughton and Laubach, 2000). Under these conditions, the surface layer is probably out of equilibrium, i.e. local production of turbulent kinetic energy (TKE) does not balance dissipation, since TKE transport might not be zero (e.g., Smeets et al., 1999).

3 Methods

3.1 Run selection according to wind regimes

We classified the GQR into three subsets corresponding to the main wind regimes (Sect. 2.3) to study characteristics of net turbulent flux for each regime during the campaign. We tried to consider as many runs as possible in each wind regime without selecting specific turbulent conditions. Hence, selection was based only on wind direction and the detection of a wind-speed maximum below the highest profile measurement.

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Runs for which wind direction was downslope (between 260 and 360°) and for which a wind-speed maximum was observed below 5 m were classified as “pure-katabatic” (42 % of the GQR). The GQR for which wind blew downslope and no maximum was observed below 5 m were classified as “downslope” (26 % of the GQR). Runs with wind direction of 45–180° were classified as “upslope” (32 % of the GQR). Throughout the text, temporal averages of a variable over the runs from one subset are noted $\langle \rangle$.

3.2 Eddy-covariance fluxes

We measured the turbulent fluxes with the two EC systems, following Eqs. (1) and (2),

$$H_{ec} = -\bar{\rho}c_p\overline{w'\theta'}, \quad (1)$$

$$LE_{ec} = -\bar{\rho}L_e\overline{w'q'} + Wpl, \quad (2)$$

where downward (upward) fluxes were set positive (negative). The ec subscript indicates flux estimates derived from the EC method, ρ is the air density (kg m^{-3}) and c_p is the specific heat of humid air ($\text{J kg}^{-1} \text{K}^{-1}$). The value of L_e was set equal to the latent heat of sublimation of the ice ($283 \times 10^4 \text{ J kg}^{-1}$) when the surface was below freezing and to the latent heat of vaporization ($250 \times 10^4 \text{ J kg}^{-1}$) when the surface was melting. The primes denote fluctuations of the variables around their 1 h means. The Webb–Pearman–Leuning term (WPL) (Webb et al., 1980) generally remained below 2 W m^{-2} throughout the campaign.

3.2.1 Potential random errors in eddy-covariance fluxes

For the EC method, the principal source of random error is poor statistical sampling of the main transporting eddies (Vickers and Mahrt, 1997). To characterize this error, we applied two different methods: Mann and Lenschow (1994) (ML) and Hollinger

and Richardson (2005) (HR) methods. The ML method assumes that temperature and vertical velocity fluctuations are joint-normally distributed. Under stable conditions, it expresses random error σ_F in the flux F as:

$$\frac{\sigma_F}{F} = \left(\frac{2\tau_f}{P} \right)^{0.5} \left(\frac{1 + r_{wx}^2}{r_{wx}^2} \right)^{0.5} \quad (3)$$

where τ_f is the integral time scale (s) of the flux, which is related to the time scale of the largest transporting eddies of the flow, P is the temporal averaging period and r_{wx} is the correlation coefficient between w and the scalar variable x associated with the flux. This method requires determining τ_f , and several methods have been proposed to calculate it (Wyngaard, 1973; Mann and Lenschow, 1994; Finkelstein and Sims, 2001). We calculated τ_f using the cospectra of w and x ; the integral time scale is given by the inverse of the frequency of the maximum in the cospectra (Wyngaard, 1973). The mean cospectra, calculated over 1 h runs and then averaged over each wind-regime subset (Fig. 2), exhibited two distinct peaks in the “downslope” and “upslope” subsets but only one in the “pure-katabatic” subset (Litt et al., 2014). The high-frequency peak is associated with small-scale fast turbulent eddies, whereas the low-frequency peak is associated with large-scale slow eddies. Within a 1 h run, fewer slow eddies are sampled than fast ones, which leads to larger random errors. Thus we allowed τ_f to change according to wind conditions: when a katabatic wind-speed maximum was found and only a single peak was observed in heat-fluxes cospectra (Fig. 2), we used the frequency of this single peak. When no maximum was detected below 5 m and two peaks were observed in the cospectra, we used the frequency of the peak found at lowest frequency, associated with the largest eddies, which control the random sampling error.

In contrast, the HR method assumes that two EC systems installed in separated locations but over similar terrain, wind conditions and fetch, measure the same flux independently. This assumption holds if they are located far enough from each other so that the largest eddies do not influence both sensors at the same time. Let F_1 be

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hourly fluxes measured with the first EC system, F_2 be those measured by the second one, and the true value of the flux be F . If the conditions described above are fulfilled, the mean value of $F_1 - F_2$ during the campaign is zero. We have ($i = 1$ or 2):

$$F_i = F + \delta F_i \quad (4)$$

5 where δF_i is the random measurement error in each flux, which is a random variable with mean 0 and standard deviation $\sigma(\delta F_i)$. Since the mean $F_1 - F_2$ is zero, the variance of $F_1 - F_2$ is equal to the variance of $\delta F_1 - \delta F_2$:

$$\sigma^2(F_1 - F_2) = \sigma^2(\delta F_1) + \sigma^2(\delta F_2) + 2 \text{cov}(\delta F_1, \delta F_2) \quad (5)$$

And then, since the δF_i are assumed to be independent, we have:

$$10 \quad \sigma(\delta F) = \frac{1}{\sqrt{2}} \sigma(F_1 - F_2) \quad (6)$$

with $\delta F = \delta F_i$. The standard deviation of δF provides an estimate of the random error in the flux. This method requires collecting enough pairs of flux samples under each reported wind condition to calculate a typical random error for each. We measured $\frac{1}{\sqrt{2}} \sigma(F_1 - F_2)$ over equally-spaced bins of wind speed over the three weeks of the campaign when both EC systems were available.

The effect of random instrumental noise on fluxes is expected to be small because the C-SAT3 and the LICOR7500 are accurate sensors with small measurement errors (Table 1). The ML and HR methods implicitly include this source of error (Businger, 1986; Billesbach, 2011), and we do not calculate its individual contribution.

20 3.2.2 Potential systematic errors on eddy-covariance fluxes

Non-orthogonal sonic anemometers may underestimate vertical wind velocity (Kochendorfer et al., 2012a; Nakai et al., 2006). Underestimates are larger when the wind-attack

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range curve that follows a $n^{-5/7}$ slope (Kaimal and Finnigan, 1994). The cospectra were adjusted over the frequency range in which the expected inertial subrange slope was observed, i.e., from their peak at $n = 5 \times 10^{-1}$ up to the frequency at which the cospectra deviated from the inertial subrange slope (Fig. 2). Between this frequency and the high frequency end at $n = 10^1$, deviations from the $n^{-5/7}$ slope were attributed to high-frequency losses (Fig. 2).

Insufficient averaging time can lead to incomplete sampling of the largest eddies and to flux losses at low frequency and thus to systematic underestimates of flux. Nevertheless, long averaging times would include spurious fluxes due to changes in the state of the turbulent flow under the effect of changes in external forcing, i.e., nonstationarity. A good choice for the averaging time-scale is a trade-off between these two constraints. To check if the 1 h averaging time-scale was appropriate, we calculated multi-resolution decomposition (MRD, Vickers and Mahrt, 2003) cospectra of w with θ and of w with q . This decomposition isolates the contributions to H and LE coming from increasing time scales as if the fluxes were estimated using increasing averaging periods. The sampling must be long enough so that the MRD cospectra fall to zero at the longest time scales considered. Another application of this method is identification of a gap scale between the time scales of fast turbulent eddies and the nonstationary fluctuations induced by the slowest motions.

3.3 Bulk-aerodynamic method

Sensible heat fluxes H and latent heat fluxes LE were estimated by applying the bulk-aerodynamic (BA) profile method between the surface and each of the 8 measurement levels of wind speed and the corresponding temperature levels from the profile mast (Table 1). The subscript ba on H and LE refers to fluxes estimated by this method. Specific humidity was calculated from relative humidity measured at the AWS and ven-

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tilated temperature profiles (see Appendix B). We have:

$$H_{\text{ba},j} = \bar{\rho} c_p k^2 \frac{\bar{u}_j (\bar{\theta}_j - \bar{\theta}_s)}{\left(\ln \left(\frac{z_j}{z_0} \right) - \psi_m \left(\frac{z_j}{L_*} \right) \right) \left(\ln \left(\frac{z_j}{z_t} \right) - \psi_h \left(\frac{z_j}{L_*} \right) \right)}, \quad (8)$$

$$\text{LE}_{\text{ba},j} = \bar{\rho} L_e k^2 \frac{\bar{u} (\bar{q}_j - \bar{q}_s)}{\left(\ln \left(\frac{z_j}{z_0} \right) - \psi_m \left(\frac{z_j}{L_*} \right) \right) \left(\ln \left(\frac{z_j}{z_q} \right) - \psi_q \left(\frac{z_j}{L_*} \right) \right)}, \quad (9)$$

5 with the same sign convention as for the EC method. The subscripts j and s refer to the j th wind-speed measurement level and the surface level, respectively. The von Karman constant k was set to 0.4. The length scale L_* is the Obukhov length, defined as

$$L_* = - \frac{\bar{\theta}_v u_*^3}{kgw' \bar{\theta}'_v}, \quad (10)$$

10 with u_* the friction velocity and the subscript v referring to virtual temperature. Stability corrections for momentum, sensible heat and humidity transfers (respectively, ψ_m , ψ_h and ψ_q) were taken from Brutsaert (1982). The different forms of these corrections are given by the following equations, where the variable x is defined as $x = (1 - 16z/L_*)^{1/4}$. If $z/L_* < 0$, we have:

$$\psi_m = 2 \ln \left[\frac{1+x}{2} \right] + \ln \left[\frac{1+x^2}{2} \right] - 2 \arctan(x) + \frac{\pi}{2}, \quad (11)$$

$$\psi_h = \psi_q = 2 \ln \left[\frac{1+x^2}{2} \right]. \quad (12)$$

If $0 < z/L_* < 1$, we have:

$$\psi_m = \psi_h = \psi_q = -5 \frac{z}{L_*}, \quad (13)$$

and if $z/L_* > 1$, we have:

$$\psi_m = \psi_h = \psi_q = -5 \left[\ln \left(\frac{z}{L_*} \right) + 1 \right]. \quad (14)$$

5 The length scales z_0 , z_t and z_q are the momentum, thermal and humidity roughness lengths (m), respectively. They were derived from least-square iterative fitting of the mean temperature and wind-speed vertical profiles (Sicart et al., 2014a) and assuming $z_q = z_t$ (Andreas, 2002). We use their median values, $z_0 = 2.07 \times 10^{-3}$ m and $z_t = 0.09 \times 10^{-3}$ m, since they did not vary significantly during the campaign.

10 3.3.1 Potential random errors in the bulk fluxes

We estimated errors of the fluxes derived from the BA method arising from random noise around the measurements both analytically and with Monte-Carlo simulations. For error propagation in the functions H and $LE = f(\Delta u, \Delta(\theta, q), z, z_0, z_{t,q})$ (Eqs. 8 and 9), we used a local linearized model, assuming that the errors were independent, normally distributed, and smaller than the partial derivatives (δ are expected measurement

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errors, and Δ are differences between the measurement height and the surface):

$$\begin{aligned}
 (\delta H)^2 = & \left(\frac{\partial H}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \left(\frac{\partial H}{\partial \Delta \theta} \right)^2 (\delta \overline{\Delta \theta})^2 + \left(\frac{\partial H}{\partial z} \right)^2 (\delta z)^2 \\
 & + \left(\frac{\partial H}{\partial z_0} \right)^2 (\delta z_0)^2 + \left(\frac{\partial H}{\partial z_t} \right)^2 (\delta z_t)^2,
 \end{aligned} \tag{15}$$

$$\begin{aligned}
 (\delta LE)^2 = & \left(\frac{\partial LE}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \left(\frac{\partial LE}{\partial \Delta q} \right)^2 (\delta \overline{\Delta q})^2 + \left(\frac{\partial LE}{\partial z} \right)^2 (\delta z)^2 \\
 & + \left(\frac{\partial LE}{\partial z_0} \right)^2 (\delta z_0)^2 + \left(\frac{\partial LE}{\partial z_q} \right)^2 (\delta z_q)^2.
 \end{aligned} \tag{16}$$

Detailed calculation of each term on the right-hand side is found in Appendix C. We assumed the stability corrections were constant under small variations $\delta \bar{u}$, $\delta \overline{\Delta \theta}$, $\delta \overline{\Delta q}$ and δz , which greatly simplifies the calculations. The effects of this simplification are discussed in Sect. 4.2.1. Values of $\delta \bar{u}$, $\delta \overline{\Delta \theta}$, $\delta \overline{\Delta q}$ and δz were adjusted according to the expected errors for wind speed, air temperature, relative humidity and height, respectively (Table 1). The manufacturer provides a value of $\delta \bar{u}$ of 1 % of the reading, but when wind speed is low, the error may not tend to zero; so, we set it to 0.1 m s^{-1} . The error in $\overline{\Delta \theta}$ was set to 0.35°C , larger than the expected thermocouple random noise ($\sigma_\theta = 0.1^\circ\text{C}$, Table 1), since $\overline{\Delta \theta}$ was affected by surface temperature errors (Appendix A). The random error in $\overline{\Delta q}$ depends weakly on the random error in air temperature and strongly on the error in relative humidity (Appendix B). We set the random error in $\overline{\Delta q}$ to 3%, equal to the error in the relative humidity. The sounding height ranger is quite accurate ($\pm 0.01 \text{ m}$), but the surface was irregular at a local scale; so, its error was set to $\pm 10 \text{ cm}$. We used δz_0 and δz_t values derived from the error analysis of Sicart et al. (2014a): $\delta \ln z_0 = \delta \ln z_t = 1.5$.

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The Monte-Carlo-based error estimate was obtained, for each measurement, by simulating 1000 dispersed measurements with a Gaussian random function whose mean equaled the measurement and whose standard deviation equaled the expected random instrumental error previously mentioned. From these dispersed data, we recalculated 1000 estimates of turbulent fluxes for each run and profile level. Random errors in mean fluxes of a subset were calculated as the interquartile range of the 1000 mean fluxes obtained from the simulated measurements.

3.3.2 Potential systematic error in the bulk fluxes

Systematic errors in the BA method could originate from systematic biases in the measurements. Air temperature can be overestimated due to heating of the shelters by shortwave solar radiation (Huwald et al., 2009). This bias was considered negligible, however, since the air-temperature shelters were continuously artificially aspirated, and residual deviations during clear-sky days were corrected using air temperature derived from the EC systems (Sicart et al., 2014a). Surface temperature measurements, derived from measurements of the longwave emission of the snow or ice surface with pyrgeometers, can be overestimated. This is due to the penetration of shortwave radiation through instrument filters and heat transfers due to heating by shortwave radiation of instrument domes (Yamanouchi and Kawaguchi, 1984). This effect was evident during the day, since estimates of surface temperature reached 1.5 °K above the melting point. We tested the impact of this bias on flux estimates by using two methods to correct it. The first method set the surface temperature to 0 °C when the raw estimate based on outgoing longwave radiation exceeded 0 °C (Sicart et al., 2008; Wagnon et al., 2003); we called this method “ T_s -blocking”. It gave an upper boundary for surface temperature. The second method was inspired by Obleitner and De Wolde (1999); we corrected the outgoing longwave emission by a percentage of SW_{inc} . We chose to use a percentage of 0.6 %, half the value of Obleitner and De Wolde (1999), since it yielded a surface temperature near 0 °C when field observations reported snow or ice melt. We called this second method “ T_s -corrected”.

The error related to the ill-defined zero reference level was studied by Sicart et al. (2014a). They showed that this effect had a weak influence on final turbulent heat fluxes, since the ablation zone of Zongo glacier remained quite smooth during the campaign.

We also studied systematic errors related to unmet theoretical requirements that could affect the BA method. First, advection or divergence of fluxes below the sensors could be high when the surface layer was not well developed, especially when a katabatic wind-speed maximum occurred at a low height under low wind-speed conditions (Litt et al., 2014). This probably led to underestimating surface fluxes when they were assessed too high above the ground, which also affected the EC method. Estimating fluxes with the BA method, applied with increasing measurement heights on the profile mast, helped us to document this issue. Second, low-frequency perturbations affected the surface-layer flow (Sect. 2.3). The additional TKE induced intermittently by low-frequency perturbations probably did not scale with mean gradients in the surface layer, potentially causing underestimates of flux (Litt et al., 2014). Comparisons with the EC-based fluxes were used to document this bias. Finally, use of inadequate stability functions could also induce biases. The most commonly used functions lead to underestimating fluxes since they do not account for intermittency under strong stable conditions (e.g. Andreas, 2002; Mahrt, 2007). These cases are related to small fluxes under weak turbulent mixing, of secondary interest for surface energy balance studies. Furthermore, this bias is expected to be small on Zongo glacier, since the mean value of the bulk Richardson number (Ri_b) (Stull, 1988) between the first and fourth profile levels was 0.07 (Sicart et al., 2014a). For this low stability, the formulas do not differ much from each other, and intermittency related to weak wind and strongly stable stratification is not a concern.

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4 Results and discussion

4.1 Eddy covariance method

4.1.1 Random error calculations

The random error in H_{ec} and LE_{ec} increased with wind speed for the Mann and Lenschow (ML) method and did not change significantly with wind speed for the Hollinger and Richardson (HR) method (Fig. 3a and b). Both methods provided similar estimates for low wind speeds below $2\text{--}3\text{ m s}^{-1}$, which represented the majority of runs ($\bar{u} < 2\text{ m s}^{-1}$ 58% of time; $\bar{u} < 3\text{ m s}^{-1}$ 88% of time). For higher wind speeds, the random error predicted with the ML method increased and was larger than that of the HR method, which remained constant. Large random errors were probably due to poor sampling of large-scale outer-layer structures, which were frequently observed in the “downslope” and “upslope” subsets when wind speed was high (Sect. 2.3). We chose to use the highest error derived from the ML method in the rest of this study.

The HR method was probably not adapted for estimating errors using the EC-mast configuration available, considering the flow characteristics observed. In “upslope” and “downslope” subsets, outer-layer eddies that interacted with the surface layer moved through the sensors in $50\text{--}100\text{ s}$ at wind speeds of about 3 m s^{-1} (Litt et al., 2014), which indicated that they were larger than the distance between the two EC systems (roughly 20 m , Fig. 1). Under these conditions, fluxes measured by the two EC systems may not be independent, since they originated from the same eddies. This is confirmed by analyzing the spectral dependence of the covariance of fluxes between the two EC systems (Fig. 3c and d). For low wind speeds in the “pure-katabatic” subset, the covariance of fluxes from both EC systems was near zero at all frequencies. For high wind speeds in the “upslope” and “downslope” subsets, significant covariance was found at low frequency ($n < 10^{-2}$), whereas near zero covariance was found at high frequency (except for the small sensible heat fluxes in the “upslope” subset). Fluxes derived from each EC system were independent at short time-scales but were not so at the time

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scale of large eddies. This may explain why HR error followed ML error at low wind speeds, but was smaller at high wind speeds. The ML method estimated the errors induced by poor sampling of the large outer-layer structures by using an adapted τ_i , whereas the HR method could not estimate it correctly.

On average, the relative random error was 34 % (Table 2) of net EC fluxes in the “pure-katabatic” subset. Relative random error was the largest (60 %) for the “downslope” subset, because net fluxes were weak for this regime, and high wind speed was associated with large random errors (Fig. 3a and b) due to the presence of outer-layer structures. Relative random error was the lowest (8 %) for the “upslope” subset, because net fluxes were the largest for this regime. Over the campaign, relative random errors derived from the ML method canceled out to a mean value of 12 %.

4.1.2 Estimates of systematic errors

Flux contributions at different attack angles for one of the EC systems are shown in Fig. 4 for selected cases whose characteristics were representative of the three wind regime subsets. Slightly higher flux was found at large attack angles in “upslope” and “downslope” cases than in the “katabatic” case, probably because the flow was gustier under strong winds in “upslope” and “downslope” cases. We found that, at most, around 30 % (19 % plus 11 %; red dotted lines in Fig. 4) of sensible heat flux was exchanged at attack angles greater than 15° . Regarding latent heat, 21 % (19 % + 2 %) of the flux was exchanged at attack angles greater than 15° . We assumed that the relation between attack angles and flux underestimation was the same for H and LE, that the fluxes exchanged at $\omega < 15^\circ$ were underestimated by 10 %, following Frank et al. (2013), and that for $\omega > 15^\circ$ the underestimation was 20 % (slightly higher than the 15 % found by Kochendorfer et al., 2012a, for the R. M. Young Sonic Anemometer). Consequently, both sensible heat and latent heat fluxes were underestimated by about 16 %, as an upper boundary.

High-frequency losses calculated from the mean cospectra of w with θ and with q were slightly more pronounced for latent than for sensible heat fluxes, probably be-

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Table 2). Similarly, the median relative random error was 35 % for the “pure-katabatic” subset. It was only 4 % for the “upslope” subset, since net turbulent fluxes were high for this subset.

4.2.2 Estimates of systematic errors

5 In the “pure-katabatic” subset, the magnitude of BA-based H , LE and their sum decreased as measurement height increased (Fig. 7). At a 2.0 m height (fifth level), sensible (latent) heat flux was 90 % (62 %) of that obtained at 0.70 m (second level). Higher up, at 5 m (eighth level), this flux was only 17 % (16 %), probably due to the shallow depth of the surface layer when a wind-speed maximum was observed at low height, around 2.0 m (Sicart et al., 2014a; Litt et al., 2014).

Vertical divergence was also observed in the “downslope” and “upslope” subsets but was significant only at heights greater than 2.0 m. We found similar latent and sensible heat fluxes at 2.0 and 0.7 m, but those at 5.0 m were only 70–80 % of those at 0.7 m. When no wind-speed maximum was observed, the surface layer was probably slightly thicker than that in the “pure-katabatic” regime, due to increased mixing induced by higher wind speeds (Sicart et al., 2014a; Litt et al., 2014), but its extent above the ground probably remained low. Nevertheless, our observations show that measurements at a 2 m height provide reliable estimates of surface fluxes in “downslope” and “upslope” wind regimes. For all wind regimes, the relative thinness of the surface layer probably also led the EC method to underestimate surface fluxes.

During the day and when the surface was not melting, surface temperature from the “ T_s -blocking” method was often slightly warmer than that from the “ T_s -corrected” method (Fig. 8). In general, the “ T_s -blocking” method predicted greater losses of turbulent energy (Fig. 9b). Averaged over the campaign, the magnitude of net turbulent fluxes estimated with the “ T_s -corrected” surface temperature was 56 % ($\approx 4 \text{ W m}^{-2}$) of that estimated with the “ T_s -blocking” surface temperature. This percentage was 64 % ($\approx 10 \text{ W m}^{-2}$) in the “upslope” subset. Because net turbulent fluxes were low in the

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surface, whereas sublimation ($LE < 0$) remained high due to large humidity gradients (Sicart et al., 2005).

For moderate-to-high wind-speed conditions ($> 3 \text{ ms}^{-1}$) in upslope and strong downslope flows, large outer-layer eddies interacted with the surface flow, and large random errors in the EC method originated from poor statistical sampling of these structures. The random error was moderate when wind speed was low. We showed that the Hollinger and Richardson (2005) method, when applied with the mast configuration of the 2007 campaign, was not adapted for deriving sampling errors due to the presence of large-scale eddy structures, because the masts were too close to each other ($\sim 20 \text{ m}$). Instead, we used the Mann and Lenschow (1994) method.

When a wind-speed maximum was observed at low-height, nonstationarity affected individual fluxes erratically and led to additional random errors in mean EC fluxes. Mean relative random error was 12 % over the campaign. Biases could lead to underestimating flux magnitude by around 20 % using the EC method. The largest bias was potential underestimation of vertical wind speed by the non-orthogonal anemometers, which could lead to underestimating fluxes by about 16 %. Such a large bias must be considered with caution, since we intentionally used large estimates. Furthermore, this issue is not well documented and remains controversial. High-frequency losses remained small, at most $\sim 4\%$.

For the BA method, the main source of random errors came from uncertainties in roughness lengths; they were large at the hourly time-scale ($\sim 40\%$) but decreased to 5 % for net turbulent fluxes estimated for the entire campaign. Systematic errors were generally high. Surface-temperature errors induced by solar radiation effects probably led to overestimating energy losses in turbulent fluxes, especially in daytime upslope flows. A larger bias arose, however, from nonstationarity induced by interactions of low-frequency perturbations with the surface layer, and dominated overall systematic errors. This led to net underestimation of flux magnitude: using the BA method, net turbulent flux over the entire campaign was only 60 % of that measured with the EC method.

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differs from that on tropical glaciers, e.g., at high latitudes and on low-altitude glaciers, where sensible heat fluxes are large but sublimation is low and deposition can be high. The role of the errors studied here might differ considerably on sites with distinctly different meteorological characteristics, and the influence of turbulent flux uncertainties on surface energy balance might also differ.

Appendix A: Surface-temperature error

Surface temperature, T_s , was derived from infrared emission from the surface. Measurements of LW_{out} include thermal emission from the surface and reflections of LW_{in} :

$$LW_{out} = \epsilon\sigma T_s^4 + (1 - \epsilon)LW_{in} \quad (A1)$$

where ϵ is thermal emissivity of the surface, and σ is the Stefan–Boltzmann constant. Inverting this relation for the surface temperature gives:

$$T_s = \left(\frac{LW_{out} - (1 - \epsilon)LW_{in}}{\epsilon\sigma} \right)^{\frac{1}{4}} \quad (A2)$$

Propagating the same way as in Eqs. (15) and (16) and considering that random errors are calculated for each variable of the expression, it yields:

$$\frac{\delta T_s}{T_s} = \frac{1}{4(LW_{out} - (1 - \epsilon)LW_{in})} \times \left((\delta LW_{out})^2 + ((1 - \epsilon)\delta LW_{in})^2 + \left(\frac{\delta \epsilon}{\epsilon} (LW_{out} - LW_{in}) \right)^2 \right)^{\frac{1}{2}} \quad (A3)$$

The Kipp & Zonen sensor notice provides an estimated error of 10 % in the irradiance (for daily sums). If we apply this as a random error in the previous equation, it yields

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unrealistically large relative error in estimates of surface temperature, i.e., as large as 6–7 K, considering a melting surface temperature of 273.15 K. Random noise must be lower; analysis of SW_{inc} and SW_{out} measurements during the night, when they should be zero, or of LW_{out} when melting is observed and thus longwave emission intensity must be constant, yields typical standard deviations of 1 or 2 W m^{-2} . This is equivalent to a random noise of 0.4 % around radiation measurements. Errors may also arise from incorrect choice of ϵ , which may change based on the state of the ice or snow surface. We consider that this error was a random error. We set the value of ϵ to 0.99 and the value of $\delta\epsilon$ to 0.01. If we consider emission from a surface at 273.15 K (315 W m^{-2}), a $\delta LW/LW$ of 0.4 % and a $\delta\epsilon$ of 0.01, Eq. (A3) yields mean random errors in surface temperature of 0.35 K. This is the value we used as the random noise around the temperature difference between the air and the surface.

Appendix B: Derivation of absolute humidity

Humidity was determined from measurements of temperature at the level considered (e.g. surface temperature when estimated at the surface), passing through the formula for change in water vapor pressure with air temperature T :

$$\bar{q}(z) = \frac{0.622e}{p} = \frac{0.622}{p} \times \overline{RH}(z) \times 6.1078 \times \exp\left(\frac{17.08055(\bar{T}(z) - 273.15)}{234.17 + (\bar{T}(z) - 273.15)}\right), \quad (\text{B1})$$

where p is atmospheric pressure (a mean of 552 hPa during the campaign) and e the saturation pressure of water in the air (hPa). To calculate profiles of \bar{q} , we assumed the air was saturated at the surface and that relative humidity decreased with height, as follows:

$$\overline{RH}(z) = \alpha \ln \frac{z}{z_q}. \quad (\text{B2})$$

We tuned α for each run in order for $\overline{\text{RH}}(z)$ to fit to the measurement of the automatic weather station (AWS) at the corresponding height. A logarithmic profile fits specific humidity measurements (Businger et al., 1971) rather than relative humidity. Currently, not much is known about RH in the surface layer of Zongo glacier. Profile measurements (Vaisala HMP45C, 2005 winter campaign, see Sicart et al., 2014a, data not shown) showed that RH decreased with height in the surface layer, but the exact shape remained unclear. We wanted to account for this decrease while keeping positive values above the unique RH measurement height at 2 m, a behavior reproduced well by a logarithmic shape. We could have done so directly on the specific humidity estimated at 2.5 m but wanted to allow for the influence of temperature variations, which were measured with the profile mast inside the surface layer.

Appendix C: Random error propagation in the bulk-aerodynamic method

C1 General formulation

We present in this appendix calculation of the terms of random error in the bulk-aerodynamic estimation of turbulent fluxes. If we assume measurement errors in each variable were independent, let us recall the formula for error in bulk flux using a linear model, assuming the stability functions were constant for small variations in Δu , $\Delta \theta$,

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Δq , z and $z_{0,t,q}$ (Eqs. 15 and 16):

$$\begin{aligned}
 (\delta H)^2 = & \left(\frac{\partial H}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \left(\frac{\partial H}{\partial \Delta \theta} \right)^2 (\delta \overline{\Delta \theta})^2 + \left(\frac{\partial H}{\partial \Delta \theta} \right)^2 (\delta \overline{\Delta \theta})^2 \\
 & + \left(\frac{\partial H}{\partial z} \right)^2 (\delta z)^2 + \left(\frac{\partial H}{\partial z_0} \right)^2 (\delta z_0)^2 + \left(\frac{\partial H}{\partial z_t} \right)^2 (\delta z_t)^2
 \end{aligned} \tag{C1}$$

$$\begin{aligned}
 (\delta LE)^2 = & \left(\frac{\partial LE}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \left(\frac{\partial LE}{\partial \Delta q} \right)^2 (\delta \overline{\Delta q})^2 \\
 & + \left(\frac{\partial LE}{\partial z} \right)^2 (\delta z)^2 + \left(\frac{\partial LE}{\partial z_0} \right)^2 (\delta z_0)^2 + \left(\frac{\partial LE}{\partial z_q} \right)^2 (\delta z_q)^2
 \end{aligned} \tag{C2}$$

where we assumed errors on the air density (thus on the air pressure measurements) were negligible. Also, the specific heat and latent heat coefficients are supposed to be accurately known. This expression can be rewritten in terms of relative error:

$$\begin{aligned}
 \left(\frac{\delta H}{H} \right)^2 = & \frac{1}{H^2} \left(\frac{\partial H}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \frac{1}{H^2} \left(\frac{\partial H}{\partial \Delta \theta} \right)^2 (\delta \overline{\Delta \theta})^2 + \frac{1}{H^2} \left(\frac{\partial H}{\partial \Delta \theta} \right)^2 (\delta \overline{\Delta \theta})^2 \\
 & + \frac{1}{H^2} \left(\frac{\partial H}{\partial z} \right)^2 (\delta z)^2 + \frac{1}{H^2} \left(\frac{\partial H}{\partial z_0} \right)^2 (\delta z_0)^2 + \frac{1}{H^2} \left(\frac{\partial H}{\partial z_t} \right)^2 (\delta z_t)^2
 \end{aligned} \tag{C3}$$

$$\begin{aligned}
 \left(\frac{\delta LE}{LE} \right)^2 = & \frac{1}{LE^2} \left(\frac{\partial LE}{\partial \bar{u}} \right)^2 (\delta \bar{u})^2 + \frac{1}{LE^2} \left(\frac{\partial LE}{\partial \Delta q} \right)^2 (\delta \overline{\Delta q})^2 \\
 & + \frac{1}{LE^2} \left(\frac{\partial LE}{\partial z} \right)^2 (\delta z)^2 + \frac{1}{LE^2} \left(\frac{\partial LE}{\partial z_0} \right)^2 (\delta z_0)^2 + \frac{1}{LE^2} \left(\frac{\partial LE}{\partial z_q} \right)^2 (\delta z_q)^2
 \end{aligned} \tag{C4}$$

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where the terms related to each relative error for each type of measurement appear independently. These terms can thus be studied separately before incorporating them back into the expression for total error.

C2 Wind-speed error

5 The relative error in wind speed propagates as follows:

$$\frac{\partial H}{\partial \bar{u}} = \rho c_p k^2 \frac{(\bar{\theta} - \bar{\theta}_s)}{\left[\ln\left(\frac{z}{z_0}\right) - \psi_m\left(\frac{z}{L_*}\right) \right] \left[\ln\left(\frac{z}{z_t}\right) - \psi_h\left(\frac{z}{L_*}\right) \right]} \quad (\text{C5})$$

$$\frac{\partial \text{LE}}{\partial \bar{u}} = \rho L_e k^2 \frac{(\bar{q} - \bar{q}_s)}{\left[\ln\left(\frac{z}{z_0}\right) - \psi_m\left(\frac{z}{L_*}\right) \right] \left[\ln\left(\frac{z}{z_t}\right) - \psi_h\left(\frac{z}{L_*}\right) \right]} \quad (\text{C6})$$

$$10 \quad \frac{1}{H} \frac{\partial H}{\partial \bar{u}} \delta \bar{u} = \frac{1}{\text{LE}} \frac{\partial \text{LE}}{\partial \bar{u}} \delta \bar{u} = \frac{\delta \bar{u}}{\bar{u}} \quad (\text{C7})$$

so that the relative error in H and LE due to errors in wind-speed measurements is simply the relative error in \bar{u} .

C3 Air-temperature error

Propagating the relative error in H due to noise in $\overline{\Delta\theta}$ gives:

$$15 \quad \frac{\partial H}{\partial \overline{\Delta\theta}} = \rho c_p k^2 \frac{\bar{u}}{\left[\ln\left(\frac{z}{z_0}\right) - \psi_m\left(\frac{z}{L_*}\right) \right] \left[\ln\left(\frac{z}{z_t}\right) - \psi_h\left(\frac{z}{L_*}\right) \right]} \quad (\text{C8})$$

So that:

$$\frac{1}{H} \frac{\partial H}{\partial \Delta\theta} \delta \overline{\Delta\theta} = \frac{\delta(\overline{\Delta\theta})}{\overline{\Delta\theta}} \quad (\text{C9})$$

Like the wind-speed error, the error due to measurement errors in temperature is simply the relative error in $\overline{\Delta\theta}$. The error due to noise around temperature indirectly affects LE via the error in measuring humidity; this is discussed later.

C4 Sensor height error

Random error in the fluxes due to random error in measuring the height can be derived as follows:

$$\frac{\partial H}{\partial z} = - \frac{\rho c_p k^2 \overline{u} \overline{\Delta\theta}}{z \left[\ln \frac{z}{z_0} - \psi_m \left(\frac{z}{L_*} \right) \right] \left[\ln \frac{z}{z_t} - \psi_h \left(\frac{z}{L_*} \right) \right]^2} - \frac{\rho c_p k^2 \overline{u} \overline{\Delta\theta}}{z \left[\ln \frac{z}{z_0} - \psi_m \left(\frac{z}{L_*} \right) \right]^2 \left[\ln \frac{z}{z_t} - \psi_h \left(\frac{z}{L_*} \right) \right]} \quad (\text{C10})$$

So that we get, for the relative error:

$$\frac{1}{H} \frac{\partial H}{\partial z} \delta z = - \frac{\delta z}{z} \left(\frac{1}{\left(\ln \frac{z}{z_0} - \psi_m \left(\frac{z}{L_*} \right) \right)} + \frac{1}{\left(\ln \frac{z}{z_t} - \psi_h \left(\frac{z}{L_*} \right) \right)} \right) \quad (\text{C11})$$

The error in height measurements likewise affects latent heat flux (changing roughness lengths and stability functions to those for humidity). The equation shows this error decreases as measurement height increases.

C5 Roughness lengths

Uncertainties in roughness lengths measurements propagate as follows:

$$\frac{\partial H}{\partial z_0} = \bar{\rho} c_p k^2 \frac{\overline{u \Delta \theta}}{z_0 \left(\ln \frac{z}{z_0} - \psi_m \left(\frac{z}{L_*} \right) \right)^2 \left(\ln \frac{z}{z_t} - \psi_h \left(\frac{z}{L_*} \right) \right)} \quad (\text{C12})$$

$$5 \frac{1}{H} \frac{\partial H}{\partial z_0} \delta z_0 = \frac{\delta z_0}{z_0 \left(\ln \frac{z}{z_0} - \psi_m \left(\frac{z}{L_*} \right) \right)} \quad (\text{C13})$$

This formula is identical for thermal and humidity roughness lengths in the case of latent heat flux.

C6 Specific humidity error

Random errors in humidity measurements affect latent heat flux as follows:

$$10 \frac{\partial \overline{LE}}{\partial \Delta q} = \bar{\rho} L_e k^2 \frac{\bar{u}}{\left[\ln \left(\frac{z}{z_0} \right) - \psi_m \left(\frac{z}{L_*} \right) \right] \left[\ln \left(\frac{z}{z_q} \right) - \psi_h \left(\frac{z}{L_*} \right) \right]} \quad (\text{C14})$$

And then:

$$\frac{1}{\overline{LE}} \frac{\partial \overline{LE}}{\partial \Delta q} \delta \overline{\Delta q} = \frac{\delta \overline{\Delta q}}{\overline{\Delta q}} \quad (\text{C15})$$

Deriving Eq. (B1), we get for the relative error in \bar{q} :

$$\frac{\delta \bar{q}}{\bar{q}} = \frac{\delta \overline{RH}}{\overline{RH}} + \frac{\delta \bar{T} \times 17.08055 \times 234.17}{\left(234.17 + (\bar{T} - 273.15) \right)^2}. \quad (\text{C16})$$

The second term on the right-hand side of the equation expresses the error in q due to errors in temperature measurements. Due to the quadratic term in the denominator, this term remains smaller than the relative error in relative humidity measurements.

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Table 1. Characteristics of the sensors from the automatic weather station, eddy-covariance systems and profile mast. Shown are random errors in measurements provided by the manufacturer and those used in this study.

Quantity	Instrument	Accuracy according to the manufacturer	Accuracy used in this study	Mean sensor height (m)
Profile Mast				
Aspirated air temperature, °C	Type-T thermocouple	0.1 °C	0.1 °C	0.1, 0.4, 0.6, 0.9, 1.2, 1.5, 1.7, 2.0, 2.7, 3.6, 4.8, 6.0
Wind speed, m s ⁻¹	Vector A100L2	1% of reading	0.1 ms ⁻¹	0.38, 0.68, 1.05, 1.58, 2.08, 2.78, 3.68, 4.88
Eddy Covariance Systems				
High-frequency wind speed components, ms ⁻¹	Campbell C-SAT3	$w: \pm 0.040 \text{ ms}^{-1}$ $u, v: \pm 0.015 \text{ ms}^{-1}$	$< \pm 0.04 \text{ ms}^{-1}$ $\pm 0.015 \text{ ms}^{-1}$	1.9 and 2.1
High-frequency sonic temperature, °C	Campbell C-SAT3	0.025 °C	0.025 °C	1.9 and 2.1
High-frequency specific humidity, %	LICOR7500	2% of reading	2% of reading	1.9 and 2.1
Automatic Weather Station				
Aspirated air temperature, °C and relative humidity, %	Vaisala HPM45C	$\pm 0.2 \text{ °C}$ 3%	$\pm 0.2 \text{ °C}$ 3%	1.0
Wind speed, ms ⁻¹	Young 05103	0.3 ms ⁻¹	0.3 ms ⁻¹	2.5
Wind direction, °	Young 05103	$\pm 3^\circ$	$\pm 3^\circ$	2.5
Incident and reflected shortwave radiation, W m ⁻²	Kipp and Zonen CM3	10% on daily sums	0.4%	0.8
Incoming and outgoing longwave radiation, W m ⁻²	Kipp and Zonen CG3	10% on daily sums	0.4%	0.8
Surface elevation changes, m	Campbell SR50	$\pm 0.01 \text{ m}$	$\pm 0.1 \text{ m}$	1.5

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Table 2. Overview of turbulent fluxes and related random errors calculated with the eddy-covariance (EC) method and bulk-aerodynamic (BA) method using the fifth level of the profile (~ 2 m height). Time occupied by the subset in the campaign (first column), net turbulent exchange ($H + LE$) for each wind regime and its ratio (%) to total net turbulent exchange of good quality runs (GQR) (second column), share of H and LE in the net exchange and mean flux exchange over the GQR (third and fourth columns). Relative random errors calculated with the Mann and Lenschow (1994) (for EC fluxes) and Monte-Carlo (for BA fluxes) methods in individual H and LE fluxes and net turbulent fluxes (fifth to seventh columns). The two last lines show results obtained for all GQR.

	Time coverage	Net turbulent exchange and ratio to total net exchange ¹	Share of turbulent exchange ² due to H	Share of turbulent exchange ² due to LE	Relative random error on $H + LE$	Relative random error on H	Relative random error on LE
Pure-katabatic	42 %	(kJ m^{-2})					
EC		3574, 15 % \pm 5 %	54 % (19 W m^{-2})	46 % (-16W m^{-2})	34 %	4 %	6 %
BA (fifth level)		-648 , 5 % \pm 2 %	46 % (6 W m^{-2})	54 % (-7W m^{-2})	35 %	6 %	4 %
Downslope	26 %	(kJ m^{-2})					
EC		-3547 , 15 % \pm 9 %	48 % (49 W m^{-2})	52 % (-54W m^{-2})	60 %	4 %	5 %
BA (fifth level)		-1256 , 9 % \pm 4 %	48 % (-31W m^{-2})	52 % (-33W m^{-2})	39 %	5 %	4 %
Upslope	32 %	(kJ m^{-2})					
EC		$-23\,554$, 100 % \pm 15 %	19 % (10 W m^{-2})	81 % (-42W m^{-2})	8 %	8 %	6 %
BA (fifth level)		$-11\,720$, 86 % \pm 6 %	21 % (6 W m^{-2})	79 % (22 W m^{-2})	4 %	6 %	4 %
Mean flux over the campaign	100 %	(W m^{-2})					
EC		-10	43 % (24 W m^{-2})	58 % (-34W m^{-2})	12 %	2 %	3 %
BA (fifth level)		-6	41 % (13 W m^{-2})	59 % (-19W m^{-2})	6 %	3 %	3 %

¹ Ratios to total net exchange were calculated as $\frac{(H+LE)_{\text{sub}}}{(H+LE)_{\text{all}}}$, where the subscripts "sub" and "all" refer to averages over the subset considered and to averages over all available runs during the campaign, respectively. The percentages after the \pm sign indicate the standard deviation of, or uncertainty in this ratio.

² The share of turbulent energy due to individual H and LE fluxes was calculated as $\frac{(H)_{\text{sub}}}{(H)_{\text{sub}}+(LE)_{\text{sub}}}$ and $\frac{(LE)_{\text{sub}}}{(H)_{\text{sub}}+(LE)_{\text{sub}}}$.

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Table 3. Evaluation of high-frequency losses in H_{ec} and LE_{ec} fluxes. Spectral adjustment: percentage of flux losses estimated by adjusting an inertial subrange on the high-frequency end of the mean cospectra of w with θ and of w with q , for the three wind regime subsets. Multi-resolution decomposition (MRD) ratio: median ratio calculated over each subset of fluxes calculated at the shortest time scale of the MRD cospectra and the flux calculated at the gap scale of the MRD cospectra.

	Method	Upslope	Katabatic	Downslope
H	Spectral adjustment	2%	2%	2%
	MRD ratio	4%	7%	6%
LE	Spectral adjustment	2%	4%	3%
	MRD ratio	2%	3%	3%

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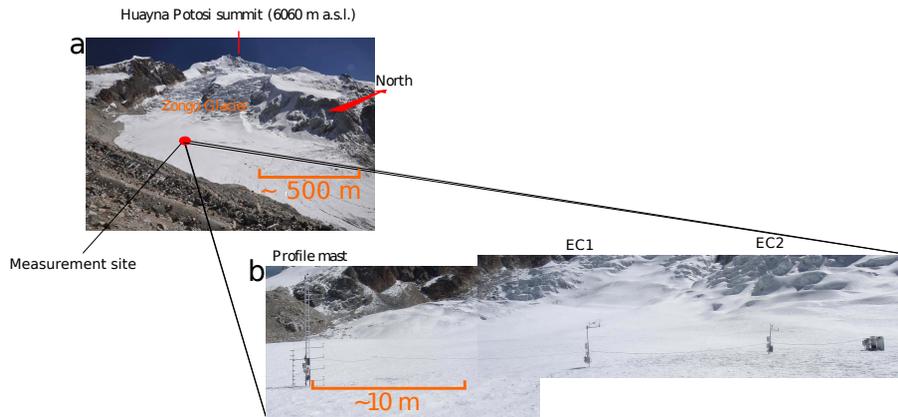


Figure 1. Overview of Zongo glacier and the instrumental set-up deployed during the 2007 dry season campaign. **(a)** Picture of the glacier, taken from the moraine at 5080 m a.s.l. The red circle indicates the location of the measurement site. **(b)** Picture of the profile mast and the eddy covariance (EC) systems. The automatic weather station, located behind the photographer, is not visible.

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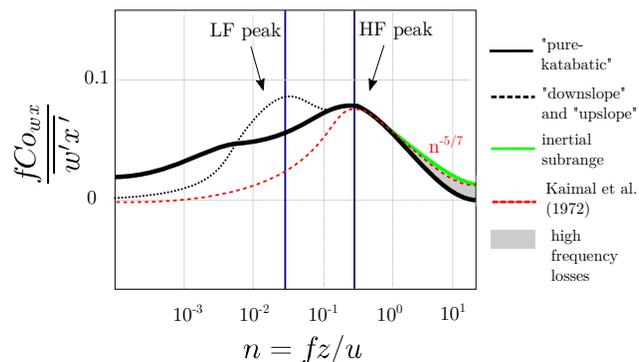


Figure 2. Cospectra of w with $x = \theta$ and of w with $x = q$ measured in the surface layer of Zongo glacier during the 2007 field campaign with one of the eddy-covariance systems (adapted from Litt et al., 2014). Cospectra were calculated over 1 h runs and then averaged over each wind regime subset. Mean cospectra for the “upslope” and “downslope” subsets (dotted black line) and the low wind speed “pure-katabatic” subset (solid black line) are presented with the inertial subrange slope (solid green curve) and the reference Kaimal curve (Kaimal et al., 1972) (dashed red curve) for comparison. The peaks used to calculate the integral length scale of the Mann and Lenschow (1994) method are identified by the vertical blue lines; LF and HF stand for high and low frequency, respectively. The high frequency losses assessed in Sect. 4.1.2 are shaded in gray.

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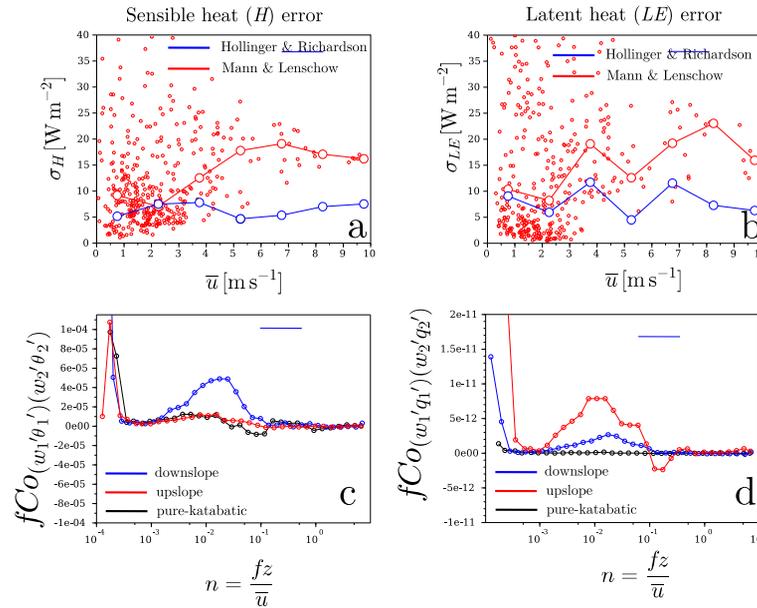


Figure 3. Random error in fluxes derived from the eddy-covariance (EC) method and covariance of fluxes between the two EC systems. **(a)** Change in the random error (W m^{-2}) in sensible heat flux H over equally spaced intervals of wind speed (width: 1 m s^{-1}). Results are from the Hollinger and Richardson (HR) method (blue line and circles) and the Mann and Lenschow (ML) method (red line and circles). Small red circles indicate estimates of the ML method for individual runs. **(b)** Results of the the HR and ML methods applied to latent heat LE estimates. **(c)** Cospectra between the $w'T'$ time series of both EC systems. Results are for downslope (blue), “upslope” (red) and “pure-katabatic” (black) subsets. Circles indicate medians of cospectral values over equally-spaced logarithmic intervals of normalized frequency. **(d)** Cospectra between the $w'q'$ time series of both EC systems, using the same notation as for $w'T'$.

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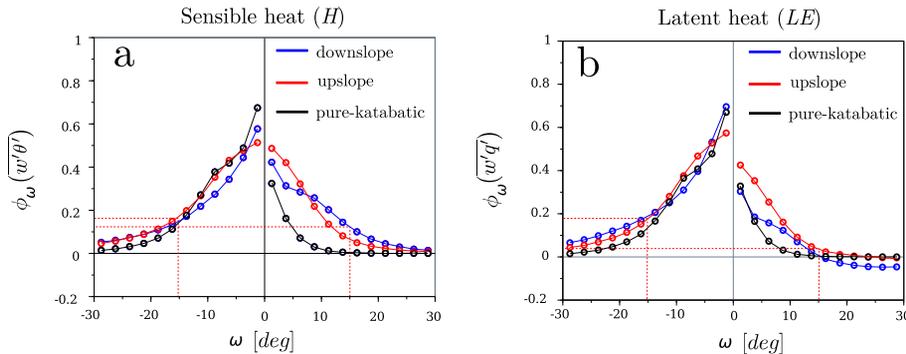


Figure 4. Cumulative contribution to fluxes H and LE (%) from different attack angles, calculated over selected events inside each of the main wind regime subsets. Flux contributions are aggregated from higher attack angles to lower attack angles. The height of the curve at a given attack angle indicates the total flux contribution at angles higher than the given angle. Cumulative contribution to **(a)** H fluxes and **(b)** LE fluxes during “pure-katabatic” (black), “downslope” (blue) and “upslope” (red) events. Red dotted lines indicate the 15° threshold and the corresponding percentage of flux.

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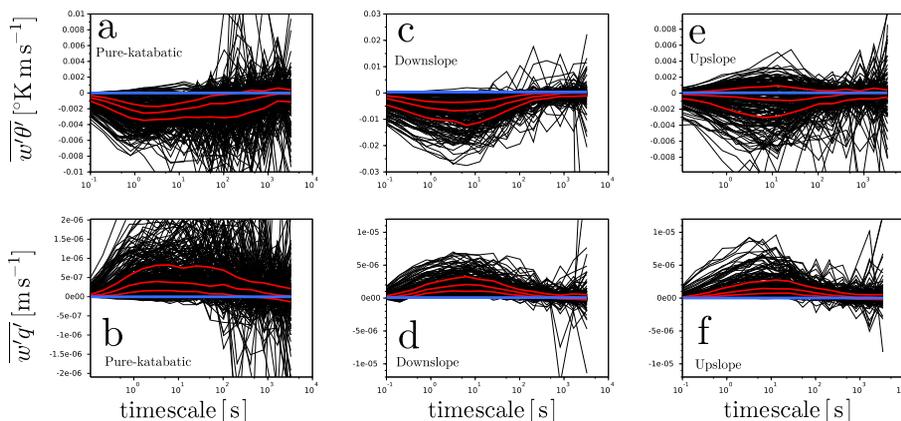


Figure 5. Multi-resolution decomposition (MRD) cospectra (black lines) of w with θ (upper panels, **a**, **c** and **e**) and of w with q (lower panels **b**, **d** and **f**) from individual runs of “pure-katabatic” (left, **a** and **b**), “downslope” (center, **c** and **d**) and “upslope” (right, **e** and **f**) wind-regime subsets. Quantiles 25, 50 and 75 of the cospectra at each dyadic time-scale calculated over a subset (red curves) and the zero line (blue line) are plotted.

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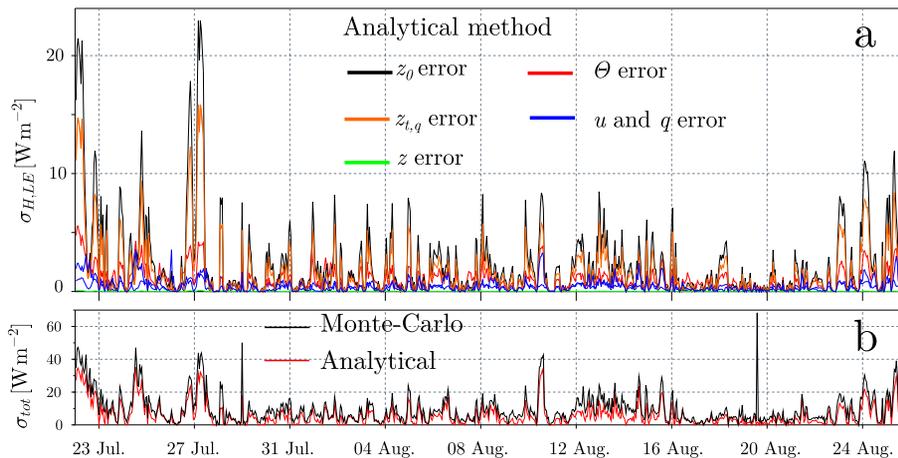


Figure 6. Results of random-error calculations using the bulk-aerodynamic method for the fifth level (~ 2.08 m) of the profile mast. **(a)** Change in individual random-error terms during the campaign estimated with the analytical method: z_0 error (black), $z_{t,q}$ error (orange), θ error (red), u and q error (blue) and z error (green). **(b)** Change in the random error in net turbulent flux during the campaign, calculated with the Monte-Carlo (black) and analytical (red) methods.

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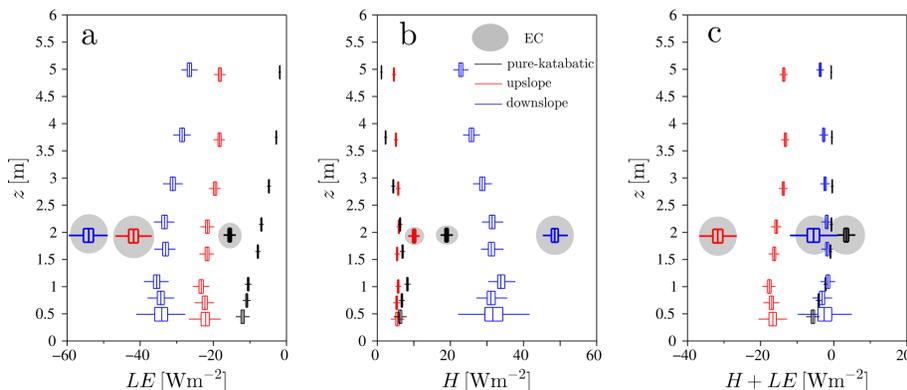


Figure 7. Mean turbulent flux exchange in the “upslope” (red), “pure-katabatic” (black) and “downslope” (blue) wind regimes estimated with the bulk-aerodynamic method and different profile mast levels, plotted against the height of measurement. Results show dispersion from Monte-Carlo simulations. The middle line in boxplots indicate the median, the boundaries of the boxes the quantiles 25 and 75 and the whiskers the quantiles 5 and 95. Boxplots of eddy-covariance (EC) flux influenced by the error estimated using the Mann and Lenschow method are highlighted in gray circles. Results are for **(a)** latent heat, **(b)** sensible heat and **(c)** net turbulent flux.

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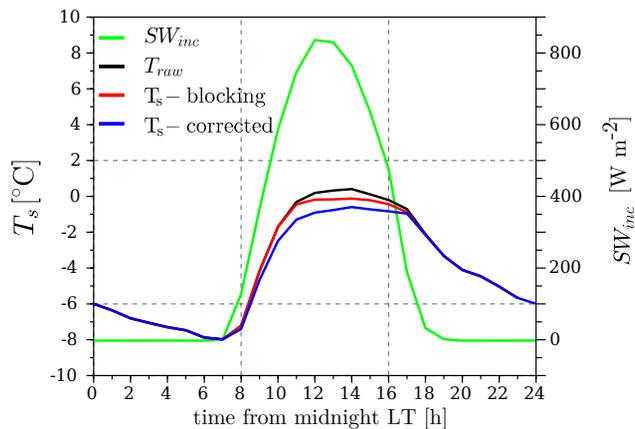


Figure 8. Mean daily cycle calculated for the entire campaign, from midnight to midnight local time (LT), of raw estimates of surface temperature (black), surface temperature derived from the “ T_s -blocking” method (red), surface temperature derived from the “ T_s -corrected” method (blue) and incoming shortwave radiation (green).

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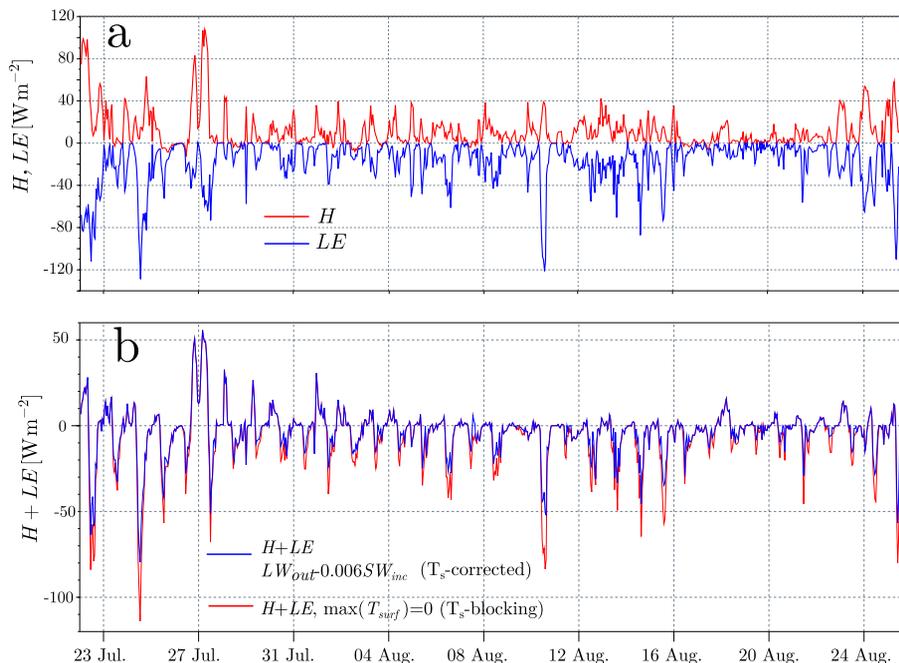


Figure 9. Turbulent fluxes derived from the bulk-aerodynamic method for the fifth measurement level on the profile mast (~ 2.08 m) with different surface-temperature derivation methods over the entire campaign. **(a)** Time-series of fluxes H and LE estimated from surface temperature derived from LW_{out} measurements corrected with the “ T_s -blocking” method. **(b)** Net turbulent flux estimated with surface temperature corrected with “ T_s -blocking” (red) and “ T_s -corrected” (blue) methods (Sect. 3).

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